

# **Ecodesign and labelling of Boilers**

## **Document 1** **Introduction**

In reaction to the first consultation forum meeting and the documents presented there, the Commission has received comments from many stakeholders and Member States. There have also been technical and relevant legislative developments at EU level, for example the recast of the Energy Performance of Buildings Directive with its Article 8 on proper installation of products. This justifies a second meeting of the consultation forum and the submission of new working documents.

The main elements in the text that you receive today:

- Combi-boilers, micro-cogeneration, and cylinders are included in the scope, as well as fossil fuelled boilers, electrical central heating, heat pumps, and solar heating.
- The proposed scope is up to 400 kW.
- The calculation model for energy efficiency has been simplified.
- Testing points have been adjusted.
- Third party testing is the norm.
- NOx emission values have been changed.
- There is a provision for co-firing of renewable energy.
- The effect of controls on energy efficiency is addressed.
- Possible problems for replacing small boilers in apartment blocks have been taking into account in setting efficiency requirements (chimney issue).

In addition, without specifying the layout format, some indicative ideas for labelling are included, to get a preliminary opinion from Member States and stakeholders pending discussions with the European Parliament and Council on the way forward regarding the label.

**Document 2**

**WORKING DOCUMENT**  
**on possible ecodesign requirements**  
**for boilers**

*Chapter 1*  
***Subject matter and scope***

1. This Regulation establishes ecodesign requirements for the placing on the market of gas-fired, oil-fired and electric boilers for hydronic central space heating (hereafter ‘Boilers’) up to 400 kW, Boilers with also a water heating function (‘Combi-boiler’) up to 400 kW and storage tanks used for central heating water or sanitary hot water (‘Cylinders’) in accordance with the definitions in Document 3. This includes Boilers also using solar energy and/or ambient heat, as well as Boilers that produce electricity as a by-product of the heat generation.
  
2. This Regulation shall not apply to the following products:
  - (a) space- and/or water heating devices within the scope of Directive 2001/80/EC on Large Combustion Plants (LCPD);
  - (b) space- and/or water heating devices using solid fuels, including biomass, as an energy source;
  - (c) space- and/or water heating devices included in and/or linked with District Heating systems (“DH”), such as large dedicated DH boilers and systems fuelled by waste heat from central power plants, waste incineration plants, larger industrial installations etcetera;
  - (d) centralised and local space heating devices based on air heating (e.g. reversible room- or centralized air conditioners);
  - (e) components placed on the market also as separate products that are not capable of performing the primary functions defined in Chapter 2. This includes but is not limited to burners, heat exchangers and controls;
  - (f) Boilers with a maximum heat output below 3.5 kW. Combi-boilers not capable of fulfilling the requirements of the smallest tapping pattern XXS as defined in Commission Regulation XX/XX/EC but with a maximum heat input above or equal to 3,5 kW shall not be evaluated on their water heating function but will be treated as boilers for space heating;
  - (g) Boilers and Combi-boilers designed for the use of biogas and/or -oil, or mixtures of fossil and bio gas/oil with a bio fuel content of 10% or more.
  - (h) Heating devices with only one CH-emitter and/or where the product itself predominantly works as the heat emitter for space heating (local heaters);
  - (i) Boilers or furnaces using vapor (steam heating systems), air (air heating systems) or other gaseous heat transfer media (e.g. some reversible air conditioner systems), boilers or furnaces supplying a heat transfer liquid with operational temperatures higher than 100 °C;
  - (j) Boilers that, either through their physical characteristics and/or through the manufacturer’s instructions, are designated to function only with CH-emitters that wholly depend on mechanically induced forced air convection for their functionality (e.g. indirect air heating systems).
  - (k) Dedicated water heaters as defined in Commission Regulation XX/XX/EC.

## *Chapter 2*

### **Definitions**

In addition to the definitions set out in Directive 2005/32/EC, the following definitions shall apply:

#### *Primary function*

1. **Boiler** means a device able to reach and maintain the indoor temperature of an enclosed space (building, dwelling, room) at a desired level under normal and extreme conditions using a hydronic heating system, in accordance with the definitions in document 3.
2. **Combi-boiler** means a device able to fulfil the primary function of a Boiler under 1) with the additional ability of heating sanitary water provided by an external grid at desired temperature levels, desired quantities, flow rates during desired intervals, in accordance with the definitions in document 3 and Commission Regulation XX/XX/EC.
3. **Cylinder** means a device able to temporarily store heat in central heating water or sanitary hot water.

#### *Physical prerequisites*

4. A **Boiler** is equipped with the means to generate heat and to transfer this heat at a single location in a building to hot water circulating in a pumped, closed-loop distribution system (CH network) with more than one heat exchanging means (CH emitter) to transfer the heating energy of the CH-water into space heating of the whole or -more commonly- several parts of a building;
5. A **Combi-boiler** is equipped as a Boiler with the additional means for heat generation and heat transfer to sanitary water.
6. A **Cylinder** is equipped with the appropriate means of storing hot water and, directly or indirectly, charging and discharging the storage tank.
7. **Heat generator** is the part of product fulfilling the physical prerequisites - in combination with a heat exchanger to transfer heat to water - for one of the following conversion processes (abbreviations in brackets):
  - (a) combustion of gaseous and/or liquid fossil fuels (FOS, FOSB);
  - (b) use of the Joule effect in electric resistance heating elements (ELBU);
  - (c) capturing solar thermal energy (SOL);
  - (d) capturing ambient heat, including but not limited to transformation processes to bring the captured heat to a higher exergy level (HP);
  - (e) heat-led cogeneration<sup>1</sup> (CHP)

Depending on the conversion process, the heat generators are denominated hereafter as FOS(a), ELBU (b), SOL (c), HP (d), CHP (e). These denominations are also used as Boolean parameters (possible values 'y'=1, 'n'=0) in the Product Information Requirements in document 4. <sup>2</sup>

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<sup>1</sup> As defined in Directive 2004/8/EC. May involve non-combustion conversion of fossil fuel to power and heat (fuel cells), explosion motors and –through combustion—Stirling engines

<sup>2</sup> A heat generator is the smallest unit for performance and energy efficiency testing and therefore an important concept for compliance testing.

8. **Preferential** heat generators in a multiple heat generator product indicate those heat generators used to the maximum of their capacity, within the restriction of the given heat demand. By definition SOL, HP and FOS are preferential and shall be used - in that order - to fill in the heat demand to the maximum of their capacity. In a multiple heat generator product, ELBU<sup>3</sup> and FOSB are **non-preferential**, i.e. by definition they fill in the remaining heat demand.
9. **Efficiency** of Boilers and Combi-boilers is the ratio between theoretical minimum heating energy demand and actual primary energy consumption expressed in gross calorific value of the fossil fuel and the primary energy equivalent of the net electricity consumed or produced in meeting aforementioned heating energy demand.
10. **Specific efficiency** of Boilers and Combi-boilers is the energy efficiency performance defined for a designated *load profile* and designated *climate* under *normal reference conditions*.
11. **Load profile** is a set of heating energy demand ('load') parameters representing the seasonal space heating or annual water heating load, based on aggregated building and installation characteristics as well as the designated climate. Depending on the size of the space or water heating demand, load profiles are denominated - from low to high - as 'XXS' (for water heating only), 'XS', 'S', 'M', 'L', 'XL', 'XXL', '3XL' and '4XL'.
12. **Climate** in this regulation is a set of representative meteorological data (e.g. outdoor temperature, solar irradiance) for representative locations in the European Union and determining –within a given physical context—the load profile and the potential for the usage of solar energy and ambient heat. For the purpose of this regulation an Average ('A'), Warmer ('W') and Colder ('C') climate are given, based on 1982-1999 weather data of Strasbourg (France), Athens (Greece) and Helsinki (Finland) respectively.
13. **Normal reference conditions** relate to the heat demand parameters for the average meteorological conditions, as opposed to **extreme reference conditions**, which relate to the peak load (maximum) demand.
14. **Designated load profile(s) or climate(s)** are (is) the load profile(s) or climate(s) for which the manufacturer declares the product fit for purpose and able to meet the Minimum Performance requirements as part of the Product Information Requirements in document 4, whereby the option to choose other climates than the Average is only relevant for products containing SOL or HP heat generator types.
15. **'Fit-for-purpose'** in this regulation is a concept exclusively depending on the manufacturer's declaration.
16. **Minimum Performance requirements** in document 4 are conditions verifying the capacity of the product to meet the heating energy demand under extreme reference conditions pertaining to the designated load profiles and - if appropriate - climate(s), in accordance with 32/2005/EC, Art. 15, sub x stipulating that ecodesign requirements shall not negatively impact the functionality of the product.
17. **Minimum Performance requirement for space heating** is the capacity of the Boiler to meet the (peak) heating power demand  $P_{design}$  in kW of the highest designated space heating load profile at design outdoor temperatures of  $-10\text{ °C}$  (Average climate),  $+2\text{ °C}$  (Warmer) and  $-22\text{ °C}$  (Colder), as specified in document 4.

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<sup>3</sup> Note that this does not exclude that in a single heat generator configuration ELBU can function as the only heat generator (e.g. electric resistance boiler).

18. **Minimum Performance requirement for water heating** is the capacity of the Combi-boiler to meet the requirements of the tapping profile pertaining to the highest designated water heating load profile as specified in Commission Regulation XX/XX/EC and characterised by a 24h sequence of draw-off with per draw-off a specified
- start time, in time h [hh:mm] elapsed from the start of the tapping pattern;
  - useful energy content of hot water to be achieved in kWh;
  - minimum flow rate in l/min;
  - useful temperature of hot water from which counting of useful energy content starts in °C;
  - minimum (peak) temperature to be achieved during tapping in °C.
19. **Specific efficiency for space heating (*etas*)** of a Boiler is the calculated energy efficiency values for a load profile and climate as defined in document 7, based on test results as given in document 6 and technical definitions in accordance with document 3. In case of SOL and air-source HP the specific efficiency for a load profile is denominated *etasA* (average climate), *etasW* (Warmer climate) and *etasC* (Colder climate), depending on the climate.
20. **Specific efficiency for water heating (*etawh*)** of a Combi-boiler is the calculated energy efficiency performance, derived from tapping pattern measurements, as defined in Commission Regulation XX/XX/EC and subsequently corrected for combi-specific factors as specified in document 3 (Technical Definitions) and document 6 (Testing). In case of SOL and air-source HP the specific efficiency for a load profile is denominated *etawhA* (average climate), *etawhW* (Warmer climate) and *etawhC* (Colder climate), depending on the climate.
21. **Energy index Cylinders** is the volume-specific (in ltrs) energy loss (in W) of the storage tank measured at an average water temperature of 60 °C and an ambient temperature of 20 °C as defined in document 4.

Additional technical definitions are set out in document 3.

### *Chapter 3* **Ecodesign requirements**

The ecodesign requirements for the covered products are set out in document 4.

### *Chapter 4* **Conformity assessment**

- The procedure for assessing conformity referred to in Article 8(2) of Directive 2005/32/EC shall be Module B as set out in Decision No 768/2008/EC as defined in Annex IV, Table 2 of said Decision.
- For the purposes of conformity assessment pursuant to Article 8 of Directive 2005/32/EC, the technical documentation file shall include the results of the calculations required in documents 5 and 6.

*Chapter 5*  
***Verification procedure for market surveillance purposes***

When performing the market surveillance checks referred to in Article 3(2) of Directive 2005/32/EC for the requirements set out in document 4, the Member State authorities shall apply the verification procedure set out in document 7.

*Chapter 6*  
***Benchmarks***

The indicative benchmarks for Boilers at the time of entry into force of this Regulation are set out in document 8.

*Chapter 7*  
***Revision***

The Commission shall review this Regulation in the light of technological progress no later than five years after its entry into force and present the result of this review to the Ecodesign Consultation Forum.

*Chapter 8*  
***Repeal***

Directive 1992/42/EC is repealed from the date of application of the first ecodesign requirements.

*Chapter 9*  
***Entry into force***

1. This Regulation shall enter into force on the twentieth day following that of its publication in the Official Journal of the European Union.
2. The ecodesign requirements set out in points 1(1) of document 4 shall apply from one year after entry into force.
3. The ecodesign requirements set out in point 1(2) of document 4 shall apply from one year after entry into force.
4. This Regulation shall be binding in its entirety and directly applicable in all Member States.

### Document 3 Technical Definitions

#### RELATING TO GENERAL BOILER DEFINITIONS IN CHAPTER 2 OF DOCUMENT 2

**Designated Load Profiles.**: Load Profile(s) for which the manufacturer declares the product fit for purpose.. Options are Load Profiles for which the product meets the minimum performance requirements as mentioned in document 4. Table II.1 gives values of  $P_{design}$  in kW pertaining to the various Load Profiles.

**Designated climates** (heating mode): Climates for which the manufacturer declares the product fit for purpose. Options are average, warmer and colder climate, corresponding to the heating season reference climates as described in Tables I.1 and I.2. Declaration of the average climate is mandatory. Declaration of the warmer and/or colder climate is optional only for boilers with SOL or air-source HP. For climates where the manufacturer declares the product not fit for purpose, no efficiency data and climate-specific tests are needed and the manufacturer will declare an “X” in positions where product information according to document 4 is required.

**Specific (seasonal) efficiency  $\eta_{tas}$**  is specific for one load profile (one  $P_{design}$  value) and expressed as

$$\eta_{tas} = L_h / Q_{tot}$$

where

- $L_h$  is the annual net heat demand in kWh/a, with  $L_h = 1000 * P_{design}$
- $Q_{tot}$  is the annual energy consumption in kWh/a

If SOL or an air-source HP are part of the product configuration the values of  $\eta_{tas}$  and  $Q_{tot}$  are climate-specific. In that case  $\eta_{tas}$  is substituted by  $\eta_{tasA}$ ,  $\eta_{tasW}$ ,  $\eta_{tasC}$  and  $Q_{tot}$  by  $Q_{totA}$ ,  $Q_{totW}$  and  $Q_{totC}$  indicating that the efficiency value relates to an Average, Warmer or Colder climate respectively.

**Annual energy consumption  $Q_{tot}$**  is the calculated annual *primary energy* consumed under *normal reference conditions*, expressed as

$$Q_{tot} = L_h + L_{sys} + Q_{gen} + Q_{el}$$

where

- $L_{sys}$  is the annual heat demand caused by system losses, which in part depend on the Boiler
- $Q_{gen}$  are the strict heat generator losses per year
- $Q_{el}$  are the losses through auxiliary energy consumption minus possible gains of electric power consumption of CHP.

If SOL or an air-source HP are part of the product configuration the values of  $Q_{tot}$ ,  $L_{sys}$ ,  $Q_{gen}$  and  $Q_{el}$  are climate-specific and those parameters will be denominated with a postscript A, W or C indicating that the parameters relate to an Average, Warmer or Colder climate respectively.



**Extreme reference space heating conditions** are defined by the heat load at outdoor temperatures of  $-10$ ,  $+2$  and  $-22$  °C for the Average, Warmer and Colder climates respectively and average EU building values. For the various Load Profiles this results in the values for  $P_{design}$  as mentioned in the Minimum Performance requirements in document 4, Table II.2.

**Normal reference space heating conditions** for all heat generators except SOL are defined by climate profiles for the EU average climate (Strassbourg), to be used for heating compliance assessment, and a warmer (Athens) and colder (Helsinki) climate, to be used for information purposes only, if the manufacturer claims that its device is suitable for either the warmer, the colder or both colder and warmer climates. The climate profiles use the ‘bins’ format.

The number of bin-hours  $hrd_j$  stems from representative weather data over the 1982-1999 period. The normal reference situation is based on heat generator operation with night-setback, therefore the hours refer to bin hours between 7:00 and 23:00h. The remainder of the load fractions is given in the first row (‘night’) of the table below.

The number of bin-hours  $hrs_j$  refers to the number of bin hours without setback (24 h profile).

The load fractions  $fracdA_j$ ,  $fracdW_j$  and  $fracdC_j$  for the average, warmer and colder climate respectively indicate the fraction of the total heating demand (‘load’) occurring in a specific bin for a specific climate. They are determined for the heating season, using the heating reference outdoor  $T_{designh}$  resulting in the expression of  $pl_j = (T_j - 16) / (T_{designh} - 16)$ . Values of  $T_{designh}$  are  $-10$ ,  $+2$  and  $-22$  for the Average, Warmer and Colder climates respectively.

The expression for  $fracdA_j$  is given below:

$$fracdA_j = \frac{hrdA_j * pl_j}{\sum_{j=1}^{46} hrdA_j * pl_j}$$

Expressions for  $fracdW_j$  and  $fracdC_j$  are as for  $fracdA_j$  but substituting  $nA_j$  for  $nW_j$  and  $nC_j$  respectively in the above expression.

For load fractions  $fracdA_j$ ,  $fracdW_j$  and  $fracdC_j$  the same expression applies, but substituting  $hrd$  values with  $hrs$  values and renaming  $fracd$  parameters with the corresponding  $fracd$  names.

Note that the ‘night’ fractions represent the situation with maximum night-setback. Actual fraction will depend on the reheat power of the boiler used at the end of the setback period to return to the normal comfort temperature (see expressions in footnote, which are part of the mathematical model in document 5).

The outdoor temperatures assumed during night setback are  $+1$ ,  $+6$  and  $0$  °C for the Average, Warmer and Colder climate respectively.

**Table I.1. Heating season reference climates, with outdoor temperature  $T_j$ , number of hours and load fraction  $frac_j$  per bin number  $j$ , with and without setback, for the Average(A), Warmer(W) and Colder(C) climate.**

		With Setback (TIM=1)						Without Setback (TIM=0)					
		hours(7.00-23.00h)			load frac			hours (24h)			load fractions(24h)		
climate-->		W	A	C	W	A	C	W	A	C	W	A	C
bin	$T_{out}$	hrdW <sub>j</sub>	hrdA <sub>j</sub>	hrdC <sub>j</sub>	fracdW <sub>j</sub>	fracdA <sub>j</sub>	fracdC <sub>j</sub>	hrsW <sub>j</sub>	hrsA <sub>j</sub>	hrsC <sub>j</sub>	fracsw <sub>j</sub>	fracsa <sub>j</sub>	fracsc <sub>j</sub>
j	$T_j$	hrs	hrs	hrs	%	%	%	hrs	hrs	hrs	%	%	%
#	°C												
<b>night[1,2,3]</b>					36,2	30,3	26,9						
9	-22			0			0,0			1			0,0
10	-21			1			0,0			6			0,3
11	-20			4			0,2			13			0,6
12	-19			11			0,5			17			0,7
13	-18			12			0,5			19			0,8
14	-17			15			0,6			26			1,0
15	-16			29			1,1			39			1,5
16	-15			32			1,2			41			1,5
17	-14			24			0,9			35			1,3
18	-13			29			1,0			52			1,8
19	-12			23			0,8			37			1,2
20	-11			27			0,9			41			1,3
21	-10		0	28		0,0	0,9		1	43		0,1	1,3
22	-9		2	28		0,1	0,8		25	54		1,3	1,6
23	-8		13	55		0,7	1,6		23	90		1,2	2,6
24	-7		12	79		0,6	2,2		24	125		1,2	3,4
25	-6		18	118		0,8	3,1		27	169		1,3	4,4
26	-5		35	137		1,6	3,4		68	195		3,0	4,9
27	-4		44	199		1,9	4,8		91	278		3,8	6,7
28	-3		56	195		2,3	4,4		89	306		3,6	7,0
29	-2		101	286		3,8	6,2		165	454		6,3	9,8
30	-1		100	285		3,6	5,8		173	385		6,2	7,8
31	0		121	243		4,1	4,7		240	490		8,1	9,4
32	1		170	364		5,4	6,5		280	533		8,9	9,6
33	2	0	193	247	0,0	5,7	4,1	3	320	380	0,3	9,5	6,4
34	3	2	218	142	0,2	6,0	2,2	22	357	228	1,8	9,8	3,5
35	4	22	210	150	1,6	5,3	2,2	63	356	261	4,7	9,0	3,7
36	5	19	190	182	1,3	4,4	2,4	63	303	279	4,3	7,0	3,7
37	6	71	211	138	4,4	4,5	1,7	175	330	229	10,9	7,0	2,7
38	7	79	213	179	4,4	4,1	1,9	162	326	269	9,1	6,2	2,9
39	8	129	253	174	6,4	4,3	1,7	259	348	233	12,9	5,9	2,2
40	9	181	235	165	7,9	3,5	1,4	360	335	230	15,7	5,0	1,9
41	10	253	236	192	9,4	3,0	1,4	428	315	243	16,0	4,0	1,7
42	11	294	163	156	9,1	1,7	0,9	430	215	191	13,4	2,3	1,1
43	12	330	144	116	8,2	1,2	0,6	503	169	146	12,5	1,4	0,7
44	13	312	123	134	5,8	0,8	0,5	444	151	150	8,3	1,0	0,5
45	14	279	86	93	3,5	0,4	0,2	384	105	97	4,8	0,4	0,2
46	15	238	66	58	1,5	0,1	0,1	294	74	61	1,8	0,2	0,1
	>15	719	203	34*	100,0			802	214	106*	116,3	113,6	
<b>total</b>		2928	3416	4368	100,0	100,0	100,0	<b>4392</b>	<b>5124</b>	<b>6552</b>	116,3	113,6	112,1
					+ [1]	+ [2]	+ [3]	<b>allhrsW</b>	<b>allhrsA</b>	<b>allhrsC</b>			

[1]=+16,3\*C<sub>tim</sub> ; [2]=+13,6\*C<sub>tim</sub> ; [3]=+12,1\*C<sub>tim</sub> with C<sub>tim</sub> is function of reheat (see text)

\* is also due to rounding errors

**Normal reference heating conditions** for solar heat generators SOL are defined by climate profiles for the EU average climate (Strasbourg), to be used for heating compliance assessment, and a *warmer* (Athens) and *colder* (Helsinki) climate, to be used for information purposes. The climate profiles use the ‘monthly’ format.

**Table I.2. Heating season reference values for SOL reference climate, with monthly values for load fraction, outdoor temperature and solar irradiance**

	Heating Season Month nr.								
	1	2	3	4	5	6	7	8	9
<b>Heat load fractions</b>									
LA_tm= (Lh+Lsys)*	0,20	0,20	0,13	0,06	0,06	0,16	0,19		
LW_tm= (Lh+Lsys)*	0,26	0,24	0,18	0,03	0,06	0,23			
LC_tm= (Lh+Lsys)*	0,17	0,17	0,14	0,09	0,04	0,03	0,08	0,12	0,16
<b>Outdoor temperature in oC</b>									
ToutA_tm	2,8	2,6	7,4	12,2	11,9	5,6	3,2		
ToutW_tm	9,5	10,1	11,6	15,3	14,5	10,4			
ToutC_tm	-3,8	-4,1	-0,6	5,2	11	12,8	6,7	1,2	-3,5
<b>Solar irradiance in W/m2</b>									
qsolmA_tm	70	104	149	192	129	80	56		
qsolmW_tm	129	138	182	227	126	110			
qsolmC_tm	22	75	124	192	234	120	64	24	13

**Annual carbon emissions C** in kg CO2 equivalent means the total estimated amount of direct and indirect carbon emissions during use and - with emissions discounted on an annual basis - end-of-life phase of the product. Direct carbon emissions depend on leakage of the refrigerant to the ambient during the use phase expressed as a fraction of the nominal refrigerant mass  $m_{refrig}$  in kg, set at 3%/year. Direct carbon emissions at end-of-life are set at 5%; discounted over a 12 year product life set at 0,4%/year. Indirect carbon emissions are set at 0,43 kg/kWh annual electricity consumption. Depending on the reference climate for heating - in case the product features a heating function - C is denominated CA (average climate), CW (warmer climate) and CC (colder climate).

The following expressions apply :

$$C = 0,43 * Q_{tot} + 0,034 * GWP^4 * m_{refrig}$$

$$CA = 0,43 * Q_{totA} + 0,034 * GWP * m_{refrig}$$

$$CW = 0,43 * Q_{totW} + 0,034 * GWP * m_{refrig}$$

$$CC = 0,43 * Q_{totC} + 0,034 * GWP * m_{refrig}$$

where the Global Warming Potential GWP in kg/kg and the refrigerant mass  $m_{refrig}$  in kg are part of the Product Information requirements, but also mandatory information items to be supplied by heat pump manufacturers under the F-gas Directive. The values of the annual energy consumption  $Q_{tot}$  are a result of the mathematical model.

<sup>4</sup> As defined in the REGULATION (EC) No 842/2006 OF THE EUROPEAN PARLIAMENT AND OF THE COUNCIL of 17 May 2006 on certain fluorinated greenhouse gases.

**Heat input** is intended as equivalent gross calorific value (Hs) of the hourly fossil fuel consumption or - in the absence of fossil fuel consumption - the electric power input for heat production.

**Primary Energy consumption in kWh** is expressed as the quantity of fossil fuel expressed in its equivalent Gross Calorific Value (upper heating value, Hs) and/or the electric energy consumed (or generated in the case of cogeneration) converted to primary energy equivalent using a primary energy conversion factor **primenergy** of 2,5. The tables below give the relevant energy parameters and their applicable tolerances.

**Table I.3. Electricity and Fossil Fuels**

Measured quantity	Unit	Value	Permissible deviation (average test period)	Uncertainty over measurement (accuracy)	of Notes
<b>Electricity</b>					
power	W			± 1 %	
energy	kWh			± 1 %	
voltage, <i>test-period &gt; 48 h</i>	V	230/ 400	± 4 %	± 0,5 %	[1]
voltage, <i>test-period &lt; 48h</i>	V	230/ 400	± 2 %		
voltage, <i>test-period &lt; 1 h</i>	V	230/ 400	± 1 %	± 0,2 %	
electric current	A			± 0,5 %	
frequency	Hz	50	± 1 %		
<b>Gas</b>					
types	-	Test gases GAD			[2]
net calorific value (NCV)	MJ/ m <sup>3</sup>	Test gases GAD		± 1 %	[3]
temperature	K	288,15		± 0,5	[3]
pressure	mbar	1013,25		± 1 %	[3]
density	dm <sup>3</sup> /kg			± 0,5 %	
flow rate	m <sup>3</sup> /s or l/min			± 1 %	
<b>Oil</b>					
<b>Heating gas oil</b>					
composition, <i>Carbon/ Hydrogen/ Sulfur</i>	kg/kg	86/13,6/ 0,2			
N-fraction	mg/kg	140	± 70		[4]
net calorific value (NCV, Hi)	MJ/kg	42,689			[5]
gross calorific value (GCV, Hs)	MJ/kg	45,55			[6]
density <b>p15</b> at 15 °C:	kg/dm <sup>3</sup>	0,85			
<b>Kerosene</b>					
composition, <i>Carbon/ Hydrogen/ Sulfur</i>	kg/kg	85/ 14,1/ 0,4			
N-fraction	mg/kg	140	± 70		[4]
net calorific value (NCV, Hi)	MJ/kg	43,3			[5]
gross calorific value (CGV, Hs)	MJ/kg	46,2			[6]
density <b>p15</b> at 15 °C:	kg/dm <sup>3</sup>	0,79			

Notes:

- [1] Test periods >48 h apply to heat pump and/or solar assisted Products. Test periods <48 h apply to conventional Products. Test period <1 h applies to the simplified test procedures for electric instantaneous water heaters
- [2] Test gases as in the essential requirements of the Gas Appliances Directive 90/396/EEC with amendments as in 93/68/EC
- [3] A factor  $K$  has to be applied to correct the calorific value for the actual average atmospheric pressure  $pa$  and gas pressure  $pg$  as well as the average gas temperature  $Tg$  over the test period.  
 $K = (pa + pg)/1013,25 + 288,15/(273,15+Tg)$
- [4] In case of low Sulfur test fuels, N-fractions lower than 70 mg/kg and lower S fractions are allowed
- [5] Default value, if value is not determined calorimetrically. Also other values are defaults. Alternatively, if volumetric mass and sulphur content are known (e.g. by basic analysis) the net heating value ( $Hi$ ) may be determined with  $Hi = 52,92 - (11,93 \times \rho_{15}) - (0,3 - S)$  in MJ/kg
- [6] Calculated from net calorific value with multiplier  $1,067 \times GCV = 1,067 \times NCV$

**Table I.4. Characteristics of reference test gases, dry gas at 15°C and 1.013,25 mbar (illustrative)**  
 [1]

Gas family and group	Designation	Composition by volume %	Net calorific value $H_i$ in MJ/m <sup>3</sup>	Gross calorific value $H_s$ in MJ/m <sup>3</sup>	Wobbe-index net $W_i$ in MJ/m <sup>3</sup>	Wobbe-index gross $W_s$ in MJ/m <sup>3</sup>	density in kg/m <sup>3</sup>	Test pressure [2] nominal, minimum and maximum in Pa		
								$p_n$	$p_{min}$	$p_{max}$
<b>1st family</b> Group a	<b>G 110</b>	CH <sub>4</sub> = 26 H <sub>2</sub> = 50 N <sub>2</sub> = 24	13,95	15,87	21,76	24,75	0,411	8	6	15
<b>2nd family</b> [3] Group H and Group E	<b>G 20</b>	CH <sub>4</sub> = 100	34,02	37,78	45,67	50,72	0,555	20	17	25
Group L	<b>G 25</b>	CH <sub>4</sub> = 86 N <sub>2</sub> = 14	29,25	32,49	37,38	41,52	0,612	25	20	30
<b>3rd family</b> Groups B/P and B [4]	<b>G 30</b>	n-C <sub>4</sub> H <sub>10</sub> =50 i-C <sub>4</sub> H <sub>10</sub> =50	116,09	125,81	80,58	87,33	2,075	29	25/ 20	35
Group P	<b>G 31</b>	C <sub>3</sub> H <sub>8</sub> = 100	88,00	95,65	70,69	76,84	1,550	50 37 50	42,5 25 42,5	57,5 45 57,5

**Notes:**

- [1] The definition, preparation and use of test gases is determined by the Essential Requirements of the Gas Appliances Directive. The table above reflects a momentary situation that may be subject to change and is for illustrative purposes only. It does not include limit gases and gases distributed nationally or locally.
- [2] Test supply pressures when no test coupling exists. Note that for Groups B/P and P two sets of test pressures are available.
- [3] Not shown is Group N (category I2N), which are as appliances using only second family gases at the prescribed supply pressure and that automatically adapt to all gases of the second family. They are tested with both G20 and G25 gases and both sets of pressure specifications.
- [4]  $p_{min} = 25$  Pa applies to group B/P;  $p_{min}=20$  Pa applies to group B. Note That "LPG" is a mixture of 3rd family gases, usually tested with test gas Group B/P or B.

**Solar energy contribution** is the global solar irradiance  $G$  in  $W/m^2$  on an optimally tilted collector surface with South orientation as defined in table II.2 multiplied with the solar heat generator efficiency characteristics as determined in accordance with document 5 and conditions described in Table I.5 below.

**Table I.5. Solar energy parameters for solar collector tests. Set values and tolerances**

Measured quantity	Unit	Value	Permissible deviation of the arithmetic mean values from set values	Permissible deviations of individual measured values from set values	Uncertainty of measurement (accuracy)	Notes
<b>Solar collector (glazed)--&gt; <math>\eta_{a0}</math>, <math>a_1</math>, <math>a_2</math> through least square curve fit for 4 x 4 test results; <math>Asol</math></b>						
Test solar irradiance (global G, short wave)	$W/m^2$	$>700 W/m^2$	$\pm 50 W/m^2$ (test)		$\pm 10 W/m^2$ (indoors)	[1]
Diffuse solar irradiance (fraction of total G)	%	$<30\%$				[2]
Thermal irradiance variation (indoors)	$W/m^2$				$\pm 10 W/m^2$	
Fluid temperature at collector inlet/outlet	$^{\circ}C/ K$	range 0-99 $^{\circ}C$	$\pm 0,1 K$		$\pm 0,1 K$	[3]
Fluid temperature difference inlet/outlet					$\pm 0,05 K$	[4]
Incidence angle (to normal)	$^{\circ}$	$<20^{\circ}$	$\pm 2 \%$ ( $<20^{\circ}$ )			[5]
Air speed parallel to collector	m/s	$3 \pm 1$ m/s			0,5 m/s	[6]
Fluid flow rate (also for simulator)	kg/s	0,02 kg/s per $m^2$ collector aperture area	$\pm 10 \%$ between tests	$\pm 1 \%$ (max dev in 1 test)		
Tilt angle	$^{\circ}$	$45^{\circ}$				
Orientation	NESW	$S \pm 45^{\circ}$				
Collector area A (absorber, gross, aperture)	$m^2$				$\pm 0,3 \%$	
Pipe heat loss of loop in test	W/K	$<0,2 W/K$				

Notes:

- Measured by pyranometer, equivalent to Class I (ISO 9060) or better. With shading ring or pyrliometer and provided with a dessicator. Regular inspection of the desiccator shall be observed. Test sample rate 30 s.
- [1] Pyranometer stays fixed in one test-point before data recording begins. Sensor shall be co-planar to collector  $\pm 1^\circ$ , at midheight of collector and receiving the same levels of direct, diffuse and reflected solar radiation as collector. When used with solar irradiance simulator minimize effect of infrared radiation at wavelength  $> 3\mu$
- [2] If  $<30\%$  can then be ignored (from EN 12975-2)
- [3] Measure within 200 mm of collector connection
- [4] Preferable accuracy  $\pm 0,02$  K
- [5] Measured by simple device: spike normal to collector and reference circles on collector plane to read spike shadow.
- [6] Measure 10 to 50 mm above collector, use artificial wind generator if  $< 2\text{m/s}$ . Check uniform distribution with anemometer. Temperature of artificial wind is ambient  $\pm 1\text{K}$ .

**Ambient heat energy contribution** is depending on the source of the HP:

- for air-source the outdoor air temperature as defined in the normal reference conditions in table II.1 and represented by test points as defined in document 5;
- for brine-source an average liquid temperature of  $0^\circ\text{C}$ ;
- for water-source an average liquid temperature of  $10^\circ\text{C}$ ;
- for ventilation air source an air temperature of  $20^\circ\text{C}$  if the flow rate does not exceed values mentioned in the notes to Table I.6 below.

**Table I.6. Energy inputs and related parameters ambient heat/ heat pumps**

Measured quantity	Unit [climate conditions]	Value	Permissible deviation (average over period)	Permissible deviations of individual measured values	Uncertainty of measurement (accuracy)	Notes
<b>Heat pump assistance: Liquid</b> (heat transfer media: brine or water)						
brine inlet temperature	$^\circ\text{C}$	0	$\pm 0,2$	$\pm 0,5$	$\pm 0,1$	
water inlet temperature	$^\circ\text{C}$	10				
volume flow	$\text{m}^3/\text{s}$ or $\text{l}/\text{min}$		$\pm 2 \%$	$\pm 5 \%$	$\pm 5 \%$	
static pressure difference	Pa		--	$\pm 10 \%$	$\pm 5 \text{ Pa}/ 5\%$	[1]
<b>Heat pump assistance: Air</b> (as heat source )						
outdoor air temperature (dry bulb)	$^\circ\text{C}$	Table II.1 and document 6	$\pm 0,3$	$\pm 1$	$\pm 0,2$	[2]
( <i>T<sub>out</sub></i> ) vent exhaust air temperature	$^\circ\text{C}$	20	$\pm 0,3$	$\pm 1$	$\pm 0,2$	
( <i>T<sub>ex</sub></i> ) mixed air temperature ( <i>T<sub>mix</sub></i> )	$^\circ\text{C}$	see note	$\pm 0,3$	$\pm 1$	$\pm 0,2$	[3]
inlet air humidity	$\text{g H}_2\text{O}/ \text{m}^3$	5,5			$\pm 5 \%$	[4]
volume flow	$\text{dm}^3/\text{s}$		$\pm 5 \%$	$\pm 10 \%$	$\pm 5 \%$	
static pressure difference	Pa		--	$\pm 10 \%$	$\pm 5 \text{ Pa}/ 5\%$	[5]

Notes:

- [1] maximum value according to manufacturer instructions shall be set at liquid pump outlet, at nominal flow rate specified. Accuracy of measurement is  $\pm 5$  Pa if value  $< 100$  Pa and 5% if value  $> 100$  Pa.
- [2] Set values apply to electric or fossil fuel fired heat pumps.
- [3] In order to avoid over-ventilation a maximum availability of ventilation exhaust air at a temperature of  $20\text{ }^{\circ}\text{C}$  is assumed, depending on the Load Profile. This parameter *ventex* [in  $\text{m}^3/\text{h}$ ] is given below. If the actual nominal inlet air flow rate *ventreal* [in  $\text{m}^3/\text{h}$ ] exceeds this value, the heat pump shall use the mixed air temperature *Tmix* [in  $^{\circ}\text{C}$ ] for testing. *Tmix* is determined from the relative proportion of exhaust air temperature *Tex* [in  $^{\circ}\text{C}$ ] and exhaust air flow rate *ventex* versus outdoor air temperature *Toutair* and the surplus air flow (*ventreal-ventex*).

In formula:  $T_{mix} = \{T_{ex} \times ventex + T_{out} \times (ventreal - ventex)\} / ventreal$

Default values *ventex* per water load profile:

parameter	unit	1 -XXS	2 -XS	3 -S	4 -M	5 -L	6 -XL	7 -XXL	8 -3XL	9 -4XL
<i>ventex</i>	$\text{m}^3/\text{h}$	109	136	128	159	190	870	1021	2943	8830

If *ventreal* is not known a default value of  $300\text{ m}^3/\text{kW}$  nominal power of heat pump can be used. Note that XXS applies to water heating only.

- [4] Note that an absolute humidity of  $5,5\text{ g}/\text{m}^3$  results in 37% Relative Humidity at  $20\text{ }^{\circ}\text{C}$  dry bulb ( $12\text{ }^{\circ}\text{C}$  wet bulb), 65% RH at  $10\text{ }^{\circ}\text{C}$  dry bulb ( $9\text{ }^{\circ}\text{C}$  wet bulb), etc.
- [5] maximum value according to manufacturer instructions shall be set at duct outlet, with heat pump not operating. Nominal air flow shall be verified. Accuracy of measurement is  $\pm 5$  Pa if value is  $< 100$  Pa and 5% if value  $> 100$  Pa.

## RELATING TO BOILER PRODUCT CONFIGURATION (BOOLEAN AND INTEGERS)

Relating to Data Inputs document 4, Table II.4.

**SOL, HP, ELBU, FOS, FOSB, CHP** are not only the denominations of the heat generators mentioned in Article 2 but also Boolean parameters (values 'y'=1; 'n'=0) indicating whether (value 'y'=1) or not (value 'n'=0) the heat generators of these types are part of the product configuration.

**Timer (TIM):** Design option of a heating regime whereby the boiler is shut down during a setback-period of 8 hours minus the time (in h) necessary to reheat the space temperature again from setback level to its normal comfort level. To apply this design option the timer parameter must be declared (TIM=yes=1) and the reheat power (parameter reheat) as a fraction of nominal radiator capacity *Pradnom*. Timer is a declared parameter and does not require the physical presence of a timing device in the Product;

**System Buffer (BUF):** Primary storage tank. If the configuration includes a primary storage tank the Boolean parameter BUF must be set to BUF=1 (otherwise BUF=0) and the manufacturer shall declare its volume *Vbuf* in litres and standing losses *Psbbuf* in W at a temperature difference between store and ambient of 40 K. Also in case ELBU is the only heat generator and using a store with volume  $> 4$  litres BUF=1 and standing losses will be declared as *Psbbuf*.

**Combi** (parameter *SOLCOMBI, HPCOMBI*) indicates whether the Boiler is also a Combi-boiler, to be declared only in case SOL or HP is part of the product configuration.

**Load profile water heating (waterload)** is the declared load profile for the Combi-boiler, characterised by the Qref values in Table III.2.



**Outdoor (FOSOUT, SOLBUFOUT, SYSBUFOUT)s:** Any Boiler or storage tank that is designated by the manufacturer to operate only outdoors. Indoors is defined as the complementary concept of outdoors, i.e. indoors is not outdoors. A designated indoors/outdoors position shall be declared for the preferential heat generator with the parameter FOSOUT and –if applicable—for the position of the solar storage tank with parameter SOLBUFOUT and/or the position of the system buffer with parameter SYSBUFOUT.

**Integrated Collector Storage (ICS):** Boolean parameter indicating whether the solar heat generator is of the ICS type; if so, the collector cannot be tested separately from the integrated storage tank.

**Heat pump main energy source (HPELEC).** Boolean parameter indicating whether the main energy source of the HP is electric ('y'=1) or fossil ('n'=0).

**Heat pump ambient heat source (HPSRC).** Numerical parameter indicating the ambient heat source, to be chosen from the following options: 1. Outdoor air. 2. Brine; 3. Ventilation air; 4. Water.

**Circulator pump options (PMP).** Numerical parameter indicating the type of circulator pump and pump configuration, to be chosen from the following options :

1. Variable speed pump & permanent magnet [option **vsd&pm**]
2. Variable speed pump, no permanent magnet type [option **vsd**]
3. Fixed speed pump [option **fixed speed**]
4. No pump, meaning there will be a stand-alone pump in the CH-circuit [option **no pump**]
5. Internal pump only, meaning a configuration with two circulators: one for a small boiler loop and another external pump for the CH-circuit [option **internal only**]

Note: Circulator efficiency will be regulated through Commission Regulation xx/xx/EC with entry date 1.1.20xx. Until that time default values for the primary energy consumption of the 5 options above are given as a fraction of **Lh** as 2, 2,5, 4, 5 and 6% respectively. After 1.1.20xx the first 3 options are taken as one integrated pump option. The values for the three options integrated pump, no pump, internal only with default values 2, 3 and 5%;

**Pump timer (tpmp).** Numerical parameter indication for the type of options for circulator pump timer control, to be chosen from the following options:

1. circulator switching off a few minutes after every burner off [option <5min],
2. circulator running all day but (almost) not in the night [option 16h];
3. circulator running 24h/day [option 24h].

**Control options (CTRL).** Numerical parameter indicating control characteristics, to be chosen from the following options (applicable values of the derived parameter **cctrl** in brackets):

1. external room temperature **ext. T-control**, i.e. boiler is delivered without room thermostat and/or outdoor sensor; to be installed in-situ (-2%);
2. external T-control **open prot** as above but boiler CPU uses an open communication protocol (-1%);
3. integrated T-control **int T-control**, boiler is delivered with room thermostat and/or outdoor sensor fitting all boiler-CPU options (0%);

4. integrated double temperature outlet **double TV**, boiler is delivered with two outlets of which the temperatures (T) and volume flow rates (V) can be regulated individually and independently, with the option to create a temperature difference between the two outlets of at least 20 K (+2%);
5. integrated multi-zone/radiator outlets **multi TV**, boiler is delivered with three or more heating water outlets of which the temperatures (T) and volume flow rates (V) can be regulated individually and independently, with the option to create a temperature difference between the outlets of at least 10 K (+4%).

#### RELATING TO PRODUCT CONFIGURATION (NUMERICAL)

**Solar collector aperture area ( $A_{sol}$ )** in m<sup>2</sup> is the collector area as established according to Best Testing Practice.

**Solar tank volume ( $V_{sol}$ )** in ltr. is the volume of the (solar part of) the solar storage tank as established according to Best Testing Practice.

**Heat transfer rate of the solar tank heat exchanger ( $U_{sol}$ )** in W/K is the maximum heat transfer of the heat exchanger in the solar tank per degree of temperature difference between heat exchanger inlet and outlet temperature as established according to Best Testing Practice. Instead of a test result a default value of  $40 \cdot A_{sol}$  may be used.

**Binlimit** in °C is the declared minimum outdoor temperature in °C required for heat pump operation.

**Turndown ratio ( $td$ ,  $tdb$ ,  $HPtd$ ):** declared ratio between the declared minimum and maximum heat input for FOS ( $td$ ) and FOSB ( $tdb$ ) or ratio between declared minimum and maximum heat output for HP ( $HPtd$ ), whereby the latter is determined for a HP tested at +12 °C outdoor temperature.

**Maximum heat input ( $Pinmax$ ,  $Pinmaxb$ )** in kW is the declared maximum fossil fuel input in equivalent Gross Calorific Value of the fuel per hour for FOS ( $Pinmax$ ) and FOSB ( $Pinmaxb$ ).

**Reheat** is the declared ratio between the heating power output for reheating after night setback and the nominal radiator capacity of the specific load profile.

**Buffer tank volume ( $V_{buf}$ )** in ltr. is the volume of the primary storage tank as established according to Best Testing Practice.

#### RELATING TO BOILER MAIN EFFICIENCY TESTS

**Test point:** Set of test conditions –energy input, ambient, etc.—at which to determine heating power output and energy efficiency of a heat generator through physical tests in accordance with document 5.

**Test results** are power and/or efficiency values resulting from tests at test points. In Table II.4 the following test values determined in accordance with document 5 are required:

- for HP the heat pump heating power outputs  **$Php$**  and the Coefficient of Performance  **$COP$**  (ratio between HP energy output and input; for other types of heat generators generally known as ‘efficiency’);
- for FOS the efficiency values  **$\eta_{ta}$** ;
- for FOSB the efficiency values  **$\eta_{tab}$**  (FOSB efficiency);

- for CHP the ratio of electric power output and FOS heat input  $P_{inmax\_chp}$  ;

**Input point:** Set of presumed energy input and/or ambient conditions for which a power output or energy efficiency value is used as an input in the mathematical model in document 6. Preliminary calculation methods to convert test point results to input point results are given in document 5.

**Input values** are power and/or efficiency values for input points obtained directly from test results or indirectly from inter-/extrapolation or other forms of aggregation. In Table II.4 the following values are determined in accordance with document 5:

- for SOL the zero-loss collector efficiency  $\eta_{a\_0}$ , first order loss coefficient  $a\_1$  and the second order loss coefficient  $a\_2$  are parameters used in a second order equation of solare collector efficiency obtained by using the least square method applied to SOL test results..
- for SOL the Incidence Angle Modifier **IAM** is a multiplier derived from an extra test at 50 ° incidence angle to the collector.
- for HP the degradation factor **Cd** is the ratio derived from the COP  $COP_{cyc}$  from an extra test at 20% cycling (6 minutes on, 24 minutes off) at conditions of  $COPI$ , a.k.a.  $COP_{max}$  in the equation for **Cd**.

#### RELATING TO BOILER AUXILIARY ENERGY

**Collector loop loss ( $U_{pipesol}$ )** in W/(m.K) is the heating power loss per meter pipe and per degree K temperature difference with the ambient, determined by Best Testing Practice.

**Solar tank standing heat loss coefficient ( $Ps_{sol}$ )** in W/K is the heating power standing loss of the solar tank, determined as parameter ‘S’ in accordance with the provisions of document 6, per degree K temperature difference between the hot water and the ambient (usually 40 K)

**System buffer tank standing heat loss coefficient ( $Ps_{buf}$ )** in W/K is the heating power standing loss of the system buffer tank, determined as parameter ‘S’ in accordance with the provisions of document 6, per degree K temperature difference between the hot water and the ambient (usually 40 K).

**Auxiliary electric power consumption** in kW: The electric power consumption in kW of the heat generator in on-mode, excluding electric power consumption of the main CH-circulator, and denominated depending on the heat generator **solaux** (SOL), **hpaux** (HP), **fosaux** (FOS), **fosbaux** (FOSB) and –indicating the electricity consumption of the charge pump—**bufaux** (BUF).

**Standby electric power consumption** in kW: The electric power consumption in kW of the heat generator in off-mode, excluding electric power consumption of the main CH-circulator, and denominated depending on the heat generator **solsb** (SOL), **hpsb** (HP), **fossb** (FOS), and **fosbsb** (FOSB).

**Fossil-fuel heat generator standby heat loss  $p\_stby$**  (FOS) or  **$p\_stbyb$** (FOSB) as a fraction of  $P_{inmax}$  (FOS) or  $P_{inmaxb}$  (FOSB) determined at 30 °C system temperature.

**Pilot flame power consumption  $P_{ign}$**  (FOS) or  **$P_{ignb}$**  (FOSB) in kW is the hourly fossil fuel consumption for the pilot flame in Gross Calorific Value equivalent of the fuel.

## OTHER BOILER-RELATED DEFINITIONS

**Variable capacity heat generator:** heat generator with the capability to vary power output the (fuel burning rate, compressor speed, etc.) whilst maintaining continuous operation. For electric heat pumps also known as ‘heat pump with inverter’;

**Staged capacity heat generator:** a heat generator with the capability to vary power output the (fuel burning rate, compressor speed, etc.) between two discrete power levels whilst maintaining continuous operation. This includes boilers with alternative burning rates set once only at the time of installation, referred to as range rating;

**Fixed capacity heat generator:** a heat generator without the capability to vary power output the (fuel burning rate, compressor speed, etc.) whilst maintaining continuous operation. This includes boilers with alternative burning rates set once only at the time of installation, referred to as range rating;

**Recoverable heat loss:** part of the heat loss from the space heating system, which may be recovered to lower the heat demand for space heating. Recoverable are for instance certain envelope losses of heat generator, system buffer, solar tank and auxiliary electric devices. Not recoverable are for instance flue gas losses, fuel losses and electricity generation losses;

**Recovered heat loss: part** of the recoverable heat loss that contributes to meet the heat demand of the space;

**Heat recovery rate** is the ratio between recoverable and recovered heat loss. The heat recovery rate depends on timing and location of the recoverable heat losses versus timing and location of the heat demand.

Note: The default heat recovery rate for parts placed indoors is 0,55 and 0 when placed outdoors. Internal parameters are *boilrecov*, *solrecov*, *bufrecov* and *auxrecov* to indicate the heat recovery rate for fossil fuel fired heat generators, solar tank standing losses, system buffer standing losses and heat from auxiliary electricity consuming devices.

**Space heating fraction (*usesol*, *usehp*)** is the share of the solar and heat pump generator energy output in the heating season partitioned to space heating in case of a combi-boiler, determined by the ratio between the space heating demand  $L_h$  and the total heating demand for space and water heating  $L_h+L_w$  in the heating season;

**Default:** Any feature or parameter value of the Product that is used as a basic reference. It does not require verification, i.e. it does not require the feature to be implemented and/or the parameter value to be valid;

**Uncertainty of measurement or measurement accuracy** is the capacity of the measurement instruments to capture the actual value of the physical parameter, expressed as maximum allowable error.

**Permissible deviations of individual measured values** is maximum/minimum permissible peak value of the physical parameter measured during the test in order for a test sample to be valid .

**Permissible deviations of the average value over the test period** (and/or the total of test samples) is the maximum/minimum permissible deviation from the prescribed setpoint of the average measured value of the physical parameter over a single test period.

Note: Usually this is the value intended if harmonised standards refer to a measurement tolerance in generic terms.

## RELATING TO COMBI-BOILER DEFINITIONS IN CHAPTER 2 OF DOCUMENT 2

*Specific efficiency for water heating  $etawh$*  of combi-boilers is specific for the designated water heating load profile (one  $P_{design}$  value) and expressed as

$$etawh = \frac{0,6 * 366 * Q_{ref}}{Q_{atotcombi}}$$

where

- $Q_{ref}$  is the reference heat demand (energy content of hot water) in kWh/d for the designated water heating profile (see values in document 4, table II.2);
- $Q_{atotcombi}$  is the annual water heating energy consumption of combi-boiler in kWh/a, with

$$Q_{atotcombi} = Q_{atot} - combicomp - combitrans$$

where

- $Q_{atot}$  is the annual energy consumption in kWh/a as defined in Commission Regulation XX/XX/EC;
- $combicomp$  in kWh/a is the heat gain for water heating from the net annual boiler envelope losses (discounted for heat recovery)  $Q_{envon}$  as calculated in document 6 for the highest declared space heating load profile;
- $combitrans$  in kWh/a is the heat gain from Passive Flue Heat Recovery Devices, i.e. devices recovering flue gas waste heat in space heating mode for use in water heating mode, determined in accordance with document 5.

If SOL or an air-source HP are part of the product configuration the values of  $etawh$ ,  $Q_{atotcombi}$ ,  $Q_{atot}$ ,  $combicomp$  and  $combitrans$  are climate-specific. In that case  $etawh$  is substituted by  $etawhA$ ,  $etawhW$ ,  $etawhC$  and  $Q_{atot}$  by  $Q_{atotA}$ ,  $Q_{atotW}$  and  $Q_{atotC}$ , etc. indicating that the efficiency value relates to an Average, Warmer or Colder climate respectively.

## Mathematical operators and expressions

+, -, *, /	addition, subtraction, multiplication, division
[X1; X2]	array (one-dimensional, with 2 elements X1 and X2)
MIN (X;Y)	if $Y \leq X$ then Y else X
MAX (X;Y)	if $Y \geq X$ then Y else X
SUM(X;Y)	X+Y
SUM(X)	if X is an array: sum of all elements in the array. If the elements of the array are indexed, e.g. with index <b>tp</b> and 7 elements then the classic notation is sigma
MIN(X;MAX(Y;Z))	$X \leq Y \leq Z$
POWER (X;Y) or $X^Y$	X to the power Y ( $X^Y$ )
LN (X)	natural logarithm of X
SIN (X)	sinus of X
COS (X)	cosinus of X
TAN (X)	tangent of X
SQRT(SUMX2PY2(X;Y))	square root of the sum of the square of X and the square of Y; $\sqrt{X^2 + Y^2}$
IF(A;X;Y)	IF expression A is True THEN X else Y (X and Y can be values or expressions)
IF(A;X;IF(C;Y;Z))	Nested IF..THEN statement: If expression A is True then X else if expression C is True then Y else Z. Represented by a table:
CHOOSE (X;Y)	X is rank number choosing element of array Y with that index
MATCH(X; A1:A3)	Result: Closest lower value matching X in array A1:A3 (cells A1, A2, A3)
INDEX([X1;X2]; X;Y)	Returns a value from a position in an array (X position only) or a table (X and Y positions)

## Document 4 Ecodesign requirements

### **1. SIGNIFICANT ENVIRONMENTAL PARAMETERS**

The following environmental aspects are identified as significant:

(a) Energy and energy-related carbon emissions in the use phase

(b) Emissions in use phase of

- i) NO<sub>x</sub>
- ii) CO
- iii) Hydrocarbons
- iv) Particulates

(c) GWP (Global Warming Potential) of refrigerant fluid used (in heat pumps) in the use and end-of-life phases.

The section dealing with minimum energy efficiency requirements relates to item (a). The paragraph 3 on emission limit values (ELVs) deals with items (b) and (c). The minimum performance requirements in paragraph 4 are a necessary boundary condition for item (a). Product information requirements are listed in paragraph 5.

### **2. MINIMUM ENERGY EFFICIENCY REQUIREMENTS**

#### **For Boilers**

As per the effective dates indicated, manufacturers shall not place on the market boilers with the following specifications:

-Boilers in size class XS, S and 10 kW maximum heat input with

- seasonal energy efficiency  $\leq 56\%$  per 1.1.2011 and
- seasonal energy efficiency  $\leq 64\%$  per 1.1.2013

-Other boilers up to 70 kW maximum heat input:

- seasonal energy efficiency  $\leq 56\%$  per 1.1.2011 and
- seasonal energy efficiency  $\leq 75\%$  per 1.1.2013

-Boilers exceeding 70 kW up to [400] kW maximum heat input:

- if as defined in Chapter 2-7 (a), (b) and (c) those with heat generator efficiency in full load  $\leq 88\%$  and in 30% part load  $\leq 96\%$ ;
- if as defined in Chapter 2-7 (d) those with heat pump efficiencies lower than the minimum criteria for promotion as outlined in the (new) RES Directive;
- if as defined in Chapter 2-7 (e) those with energy performance lower than the minimum high efficiency criteria as outlined in the CHP Directive.

Additional requirements for the placing on the market of boilers exceeding 70 kW maximum heat input are:

1. As from 1/1/2013 Boilers with heat generation only by combustion of gaseous and/or liquid fuels may only be installed if the heating system also includes controls and other components which bring the overall energy heating system efficiency rating above 96% (Local or National legislation may specify a higher level). This will imply the use of renewables or high efficiency cogeneration.
2. Boilers shall be placed on the market with monitoring equipment (including data recording) allowing real life efficiency of the heat emitter (and emissions) to be estimated for compliance assessment of the installation with applicable regulations.

Recording:

- Water feed and return temperatures,
- water flow rates (pump settings),
- energy input (from burner settings)
- Flue gas monitoring (CO/CO<sub>2</sub>/O<sub>2</sub> + temperature etc.)

This should include a suitable interface (e.g. GSM protocol) allowing equipment owner, enforcement authorities, etc. to download data periodically, once a suitable standard for this purpose shall have been published in the Official Journal to ensure interoperability. A mandate for such a harmonised standard will be issued with a view to achieve interoperability.

In the context of the EPBD, for boilers exceeding 70 kW up to [400] kW maximum heat input, furthermore a minimum seasonal energy efficiency requirement of 75 % per 1.1.2011 and 95 % per 1.1.2013 should be considered by the Member States.

### For Combi-boilers

The table below gives the minimum specific efficiency  $\eta_{wh}$  in %. The efficiency is to be determined in accordance with Commission Regulation XX/XX/EC, corrected in accordance with the provisions in document 5.

**Table II.1 . MEPS for Combi-boiler, minimum specific efficiency  $\eta_{wh}$  in %**

Load profile water heating	XXS	XS	S	M	L	XL	XXL	3XL	4XL
From 1.1.2011	29	32	32	39	46	50	60	64	64
From 1.1.2013	32	35	35	45	56	62	72	80	86

### For Cylinders

From 1 January 2011, the requirement on standing loss is as follows

$$S < 20 + 0,25 \times V$$

Where

S is the standing loss in Watts



V is the nominal capacity in litres

Standing loss is assessed for an ambient temperature of 20 °C and a hot water temperature of 60 °C according to Best Testing Practice.

Note: Most common and acceptable is the measurement of the electric power consumption of an immersed electric water heater (added or already incorporated) at thermal equilibrium for the temperatures mentioned. Alternatively, the storage tank with 20 °C water (ambient) may be charged to a set temperature of 60 °C and the energy input is measured. After 24h the tank is discharged and the energy content (temperature, volume) of the hot water (with reference to ambient) is measured. The difference between the two measurements, divided by 24h, is the standing loss in W.

Guidance documents for compliance assessment are given in document 7.

### 3. EMISSION LIMIT VALUES

The following emissions in the use phase are identified as significant:

- NO<sub>x</sub>
- CO
- Hydrocarbons
- Particulates
- Refrigerant fluids in heat pumps

For NO<sub>x</sub> emissions in the use phase of Boilers during space heating, assessed according to best testing practice the following emission limit values will apply:

- From 01/01/2013: 50 mg/kWh for gas boilers
- From 01/01/2014: 105 mg/kWh for oil boilers

For boilers with electricity output (that is, cogeneration units) a credit for displaced NO<sub>x</sub> from central power plants and avoided grid losses will be added to the amount of admissible NO<sub>x</sub> emissions<sup>5</sup>:

- From 01/01/2013: 50 mg/kWh for gas Gross Caloric Value input
- From 01/01/2013: 75 mg/kWh for oil Gross Caloric Value input

For NO<sub>x</sub> emissions in the use phase of Combi-boilers during water heating, assessed according to best testing practice the emission limit values of Dedicated Water Heaters as defined in Commission Regulation XX/XX/EC will apply. The same NO<sub>x</sub> credit as indicated above can be applied for the electricity produced during water heating by cogeneration Combi-boilers.

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<sup>5</sup> Based on the emission values in the Directive on Large Combustion Plants for gas power plants in the range of 50-500MW and assuming an electric output of 15 % as in the best Stirling engines.

For emissions of CO, hydrocarbons and particulates current harmonised measurement methods should be improved as they currently only address steady state mode. The general requirements under the product safety and gas appliance Directives shall apply where applicable to the covered products.

The Commission will issue a mandate to the harmonisation bodies to develop appropriate measurement standards.

#### 4. MINIMUM PERFORMANCE REQUIREMENTS

In order to avoid negative impact on the functionality of the product in accordance with Art. 15, sub x of 2005/32/EC, the following will apply:

For Boilers the maximum power output under design conditions  $P_{maxdesign}$  shall be higher than or equal to the design power  $P_{design}$  of the space heating Load Profile(s) declared.

$P_{maxdesign}$  is to be determined in accordance with document 6.

Values of  $P_{design}$  are given in the table below

**Table II.2**

Load Profile space heating	XS	S	M	L	XL	XXL	3XL	4XL
$P_{design}$ in kW	3,5	5,3	8	12	18	27	41	60

For Load Profiles up to XXL, the maximum heat input is 70 kW. For Load Profiles 3XL and 4 XL the maximum heat input is 100 and 150 kW respectively.

Combi-boilers must be able to meet all requirements of the tapping profile as defined in Commission Regulation XX/XX/EC on Dedicated Water Heaters, pertaining to water heating Load Profile declared.

For illustrative purposes the table below recites Commission Regulation xx/xx regarding the daily heating energy content of the hot water to be delivered  $Q_{ref}$ .

**Table II.3**

Load Profile water heating	XXS	XS	S	M	L	XL	XXL	3XL	4XL
$Q_{ref}$ in kWh/d	2,1	2,1	2,1	5,85	11,7	19,1	24,5	46,8	93,52

All products in the scope will be subject to a "fit for purpose" (see Chapter 2-15) evaluation in line with the product definitions in Article 2 and according to Best Testing Practice.

## 5. PRODUCT INFORMATION REQUIREMENTS

On 1 January 2011, the information of the covered products, set out in points below, shall be visibly displayed:

- (a) In the technical documentation of the product;
- (b) On free access websites of the manufacturers an/or importers;

As regards to the technical documentation, the information as specified in document 9 (Energy labelling requirements) must be provided.

In addition the data below must be reported in the technical documentation as specified below. The exact wording used in the list does not need to be repeated. It may be displayed using graphs, figures or symbols rather than text.

For Boilers the manufacturer shall specify the main conventional energy source (gas, oil or electric) and provide additional product information requirements given in the following table.

As from 1/1/2013 Boilers with heat generation only by combustion of gaseous and/or liquid fuels shall be supplied with the following message: *"This Boiler shall only be installed if the heating system also includes controls and other components which bring the overall energy heating system efficiency rating above 96% (Local or National legislation may specify a higher level). This will imply the use of renewables or cogeneration"*.

Definitions of the parameters mentioned are given in documents 3 and 6.

**Table II.4a. Product Information Requirements Boilers (Data Inputs)**

<b>IDENTIFICATION</b>		<b>unit</b>	<b>MAIN EFFICIENCY TESTS</b>		<b>unit</b>
<b>1</b>	Manufacturer		<b>35</b>	Zero-loss coll. efficiency eta_0	-
<b>2</b>	Brand & Model name		<b>36</b>	First-order loss coefficient a_1	W/(m <sup>2</sup> K)
<b>3</b>	Date (year of manufacture)		<b>37</b>	Second-order loss coefficient a_2	W/(m <sup>2</sup> K <sup>2</sup> )
<b>4</b>	Designated climate(s)	1-3	<b>38</b>	Incidence angle modifier IAM	-
<b>5</b>	<b>SPACE HEATING LOAD PROFILE(S)</b>	1-8	<b>39</b>	etasol (for ICS only)	
	<b>CONFIGURATION</b>			<b>HP</b>	
	<b>Declared Boolean or discrete options</b>		<b>40</b>	Php5 in kW / COP5 (2 values)	kW / [-]
	<b>ALL</b>		<b>41</b>	Php4 in kW / COP4 (°)	kW / [-]
<b>6</b>	solar? SOL	y/n	<b>42</b>	Php3 in kW / COP3 (°)	kW / [-]
<b>7</b>	heat pump? HP	y/n	<b>43</b>	Php2 in kW / COP2 (°)	kW / [-]
<b>8</b>	electric back-up ELBU	y/n	<b>44</b>	Php1 in kW / COP1(°)	kW / [-]
<b>9</b>	fossil fuel? FOS	y/n	<b>45</b>	COPcyc (20%Php1)	[-]
<b>10</b>	fossil fuel? FOSB	y/n		<b>FOS*</b>	
<b>11</b>	micro-cogeneration? CHP	y/n	<b>46</b>	eta4 (per load profile)	
	<b>SOL</b>		<b>47</b>	eta3 (°)	
<b>12</b>	SOL+hot water? SOLCOMBI	y/n	<b>48</b>	eta2 (°)	
<b>13</b>	solar tank outdoors? SOLBUFOUT	y/n	<b>49</b>	eta1 (°)	
<b>14</b>	integrated collector+store? ICS	y/n		<b>FOSB</b>	
	<b>HP</b>		<b>50</b>	_etab4	
<b>15</b>	HP+hot water? HPCOMBI	y/n	<b>51</b>	_etab3	
<b>16</b>	HP electric? HPELEC	y/n	<b>52</b>	_etab2	
<b>17</b>	HPsrc (air, water, brine, vent.airmix)	1-4	<b>53</b>	_etab1	
	<b>FOS</b>			<b>CHP</b>	
<b>19</b>	FOS generator outdoors? FOSOUT	y/n	<b>54</b>	_chp4	
	<b>other</b>		<b>55</b>	_chp3	
<b>18</b>	SOL/HP water heat load? waterload	1-9	<b>56</b>	_chp2	
<b>20</b>	system buffer? BUF	y/n	<b>57</b>	_chp1	
<b>21</b>	setback timer? TIM	y/n		<b>AUXILIARY ENERGY TESTS</b>	
<b>22</b>	Pump configuration? PMP	1-5		<b>SOL</b>	
<b>23</b>	Pump timer? tpm	1-3	<b>58</b>	Coll. loop loss per m pipe Upipesol	W/(m.K)
	<b>Declared numerical</b>		<b>59</b>	Tank heat loss coeff Psbsol	W/K
	<b>SOL</b>		<b>60</b>	Solar pump power solaux	W
<b>25</b>	SOL collector aperture area? Asol	m <sup>2</sup>	<b>61</b>	Solar standby solsb	W
<b>33</b>	SOL tank volume (solar part)? Vsol	ltr		<b>HP</b>	
<b>34</b>	UA-value of heatexchanger UAsol	W/K	<b>62</b>	HP aux. Power hpaux	W
	<b>HP</b>		<b>63</b>	HP standby power hpsb	W
<b>26</b>	HP max. outdoor temp.? binlimit	oC		<b>FOS</b>	
<b>27</b>	HP turndown ratio? Hptd		<b>64</b>	fos standby heat loss p_stby	kW
	<b>FOS</b>		<b>65</b>	pilotflame power Pign	kW
<b>28</b>	FOS max. heat input? Pinmax	kW	<b>66</b>	El. at Poff fossb	W
<b>30</b>	FOS turndown ratio? td		<b>67</b>	El. at Pmin elmin	W
	<b>FOSB</b>		<b>68</b>	El. at Pmax elmax	W
<b>29</b>	FOSB max. heat input? Pinmaxb	kW		<b>FOSB</b>	
<b>31</b>	FOSB turndown ratio? tdb		<b>69</b>	fosb standby heat loss p_stbyb	kW
	<b>other</b>		<b>70</b>	El. at Poff fosbsb	W
<b>32</b>	BUF tank volume? Vbuf	ltr	<b>71</b>	El. at Pmin elminb	W
<b>24</b>	TIM reheat power (%Pradnom)		<b>72</b>	El. at Pmax elmaxb	W
				<b>other</b>	
			<b>73</b>	Buffer tank ref. heat loss Psbbuf	W/K

**Table II.4b. Product Information Requirements Boilers continued (Data Outputs)**

**For each declared Load Profile and –in case of SOL or air-source HP- each designated climate .**

<b>74</b>	Annual space heating load	kWh/a
<b>75</b>	Annual primary energy consumption	kWh/a
<b>76</b>	Specific energy efficiency	kWh/a
<b>77</b>	Annual electricity production	kWh/a

**Only for the highest declared Load profile**

<b>78</b>	NOx emissions	mg/kWh
	GWP refrigerant (only for heat pump, obligation under F-gas directive; IPPC value)	kg CO2 eq./kg
<b>79</b>		
<b>80</b>	Annual carbon emission	kg CO2 eq./a

*\*= Note that for FOS the values for  $\eta_{a1}$ ,  $\eta_{a2}$  and  $\eta_{a4}$  correspond to test point results for the highest declared load profile. For the same boiler up to 2 extra load profiles can be declared using the results from two additional test points ( $\eta_{a2hot}$ ;  $\eta_{a1hot}$ ). The value for  $\eta_{a3}$  in the highest declared load profile and –if appropriate-- the efficiency values in the other load profiles are determined through inter-/extrapolation.*

Additionally, the manufacturer shall provide general information about the declared Load Profiles in order to help consumer and installer to select the right capacity:

**Table II.5 . General information on Load Profiles**

- a) Radiator nominal capacity  $P_{radnom}$  in kW, defined as the heat output at a heating regime of 75/65/20 °C for feed, return and ambient temperature with  $P_{radnom}=1,66 P_{design}$ ,
- b) Nominal radiator flow rate  $nomflow$  in kg/h pertaining to  $P_{radnom}$  with  $nomflow=86,2 P_{design}$
- c) Annual net space heating demand of the dwelling or building  $L_h$  in kWh/a with  $L_h=1000 P_{design}$ ;
- d) Indicative value for the floor area of an existing dwelling or building  $F_{exist}$  in m<sup>2</sup> with  $F_{exist}=10,87 P_{design}$
- e) Indicative value for the floor area of a new dwelling or building  $F_{new}$  in m<sup>2</sup> with  $F_{new}=28,57 P_{design}$

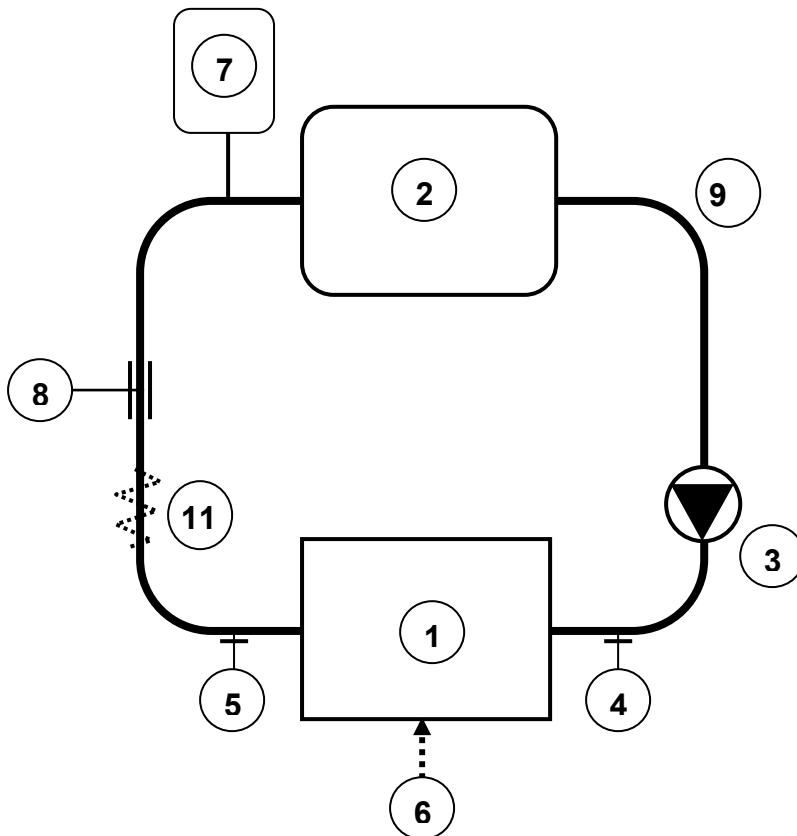
Note that the values for  $F_{exist}$  and  $F_{new}$  are default values for average EU. Instead national values for the conversion from  $P_{design}$  may be used, issued by the national authorities in the countries where the product is placed on the market. In that case the source of information and the area for which these values are valid must be mentioned.

**Document 5**  
**Testing Methods**

This section deals with the specification of test points and test results defined in document 3 and referenced in the Product Information Requirements in Document 4. Also it specifies preliminary calculation methods to derive input data for input points as required in the energy efficiency calculation in document 6.

**GENERAL TEST SET-UP**

The diagram below shows the generic test rig for hydronic heat generators, consisting of a circuit with a well-insulated pipe 9, in which water is circulating -driven by a circulator pump 3- between the heat generator 1 and a cooler/heat exchanger 2. The system return temperature  $T_{return}$  is measured just (indicatively 10-20 cm) before the heat generator at point 4 and the system feed temperature  $T_{feed}$  is measured just (indicatively 10-20 cm) after the heat generator at point 5. Rapid-response temperature sensors shall be used. During the test the mass flow rate of the heated water is determined by a high-precision mass (or volume) flow sensor 8. <sup>6</sup>



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<sup>6</sup> Flow rate measurement by temporarily tapping water from the loop after the heat generator and letting in water at  $T_{return}$  before the heat generator is still allowed as an alternative (currently hardly in use).

1. Boiler/ heat generator
2. Cooler/ heat exchanger, typically with large buffer capacity for temperature stabilisation
3. Circulator pump
4. Return temperature ( $T_{\text{return}}$ ) sensor
5. Feed temperature ( $T_{\text{feed}}$ ) sensor
6. Boiler energy input
7. Expansion vessel to maintain water pressure in the loop
8. Flow sensor
9. Loop

General ambient conditions are defined by ambient temperature, (local) air speed, heating water temperature and flow rate, as indicated for indoor tests in the table below. For conditions at outdoor tests see section on solar heat generators.

Table IV.1. General test conditions and outputs. Set values and tolerances

Measured quantity	Unit	Value	Permissible deviation (average over test period)	Permissible deviations of individual measured values	Uncertainty of measurement (accuracy)	Notes
<b>Ambient</b>						
ambient temperature indoors <i>other</i>	°C/ K	$20 \pm 2 \text{ } ^\circ\text{C}$	$\pm 1 \text{ K}$	$\pm 2 \text{ K}$	$\pm 0,1 \text{ K}$	
maximum air speed <i>HP</i> (at HP off)	m/s	<1,5 m/s				
maximum air speed <i>other</i>	m/s	<0,5 m/s				
<b>Time</b>						
Minimum sample rate SOLAR tests	s	30s			$\pm 0,2 \%$	
<b>system water</b>						
water temperature during test <i>other</i>	°C/ K	$T_{\text{feed}}/T_{\text{return}}$	$\pm 0,5 \text{ K}$	$\pm 1 \text{ K}$	$\pm 0,2 \text{ K}$	[1]
volume flowrate <i>HP</i>	dm <sup>3</sup> /s		$\pm 5 \%$	$\pm 10\%$	$\pm 1 \%$	
volume flowrate <i>other</i>	dm <sup>3</sup> /s				$\pm 1 \%$	

Notes:

[1] To be measured by "rapid response thermometer", meaning an instrument that registers within 1 s. at least 90% of the final temperature rise from 15 to 100 °C when the sensor is plunged in still water.

Minimum dimensions of the test room as well as the construction of the platform on which the heat generator is to be mounted to shield it from external influences shall be according to Best Testing Practice.

## TEST PROCEDURE EFFICIENCY AND PERFORMANCE TESTS

Tests are performed after thermal equilibrium with the appropriate temperatures, flow rate and energy in- and outputs is reached.

The product of the supplied mass, temperature difference between  $T_{\text{return}}$  and  $T_{\text{feed}}$  and the specific heat capacity of the heating water delivered during the test period is defined as the heat output  $Q_{\text{out}}$  in kWh. The energy input to the heat generator  $Q_{\text{in}}$  in kWh is the electric energy consumption during the test and/or the product of the mass/volume of the fossil fuel delivered at reference conditions and its gross calorific value GCV (a.k.a. upper heating value,  $H_s$ ). Power input  $P_{\text{in}}$  and power outputs  $P_{\text{out}}$  relate to ratios of energy in- and outputs and the test period. Test point efficiency is defined as the ratio of power output and input.

Possible renewable heat inputs, i.e. solar irradiation and/or ambient heat, shall be supplied to the heat generator at the required test conditions.

In case the prescribed volume flow rate during the test is small and/or the test is conducted in outdoor conditions, e.g. with solar heat generators, the test rig may not necessarily be a loop, provided that the water flowing in the heat generator is supplied at the required  $T_{\text{return}}$  water temperatures.

The circulator pump used during the test may be a separate pump or an integrated pump delivered with the heat generator.

Accuracy and tolerance levels for the energy inputs as defined in document 3 and the underlying document 5 apply.

Efficiency and performance test results are corrected for:

- Heat gain by the circulator pump, determined through an additional test or from a default deduction of 55% of the average pump electricity consumption during the test. The pump heating power is to be deducted from the measured power output  $P_{\text{out}}$  before calculation of the energy efficiency of a test point.
- Deviations from reference conditions for the energy inputs and outputs as defined in document 3.

Depending on the type of heat generator, test conditions are specified by combinations heat generator power input or –output, system feed, return and/or average temperatures and/or flow rates. For renewable energy sources additional requirements as specified below for ambient or solar energy inputs apply.

Depending on the type of heat generator tests shall be performed at between 4 and 6 different test points with specific efficiency values.



## TEST POINTS AND PRELIMINARY CALCULATIONS

### SOLAR COLLECTOR TESTS

For solar collectors at least 4 x 4 tests, with 4 different collector inlet temperatures  $t_{in}$  evenly spaced over the operating range and 4 test samples per collector inlet temperature are measured to obtain test values for the water outlet temperature  $t_o$ , the ambient temperature  $t_a$ , the solar irradiance  $G$  and the measured efficiency at the test point  $\eta$ <sup>7</sup>. If possible, one inlet temperature shall be selected with  $t_m = t_a \pm 3K$  to obtain an accurate assessment of the zero-load efficiency  $\eta_0$ . With fixed collector (no automatic tracking) and test conditions permitting, two test samples should be done before solar noon and 2 after. Maximum temperature of the heat transfer fluid (i.e. the top of the operating range) shall be  $>80^\circ C$ .<sup>8</sup> The recommended maximum value of the reduced temperature difference  $T_m^*$  is  $>0,09 \text{ m}^2\text{KW}^{-1}$ .

The flow rate during the tests is a given (70 l/h, see Table 2).

For the instantaneous collector efficiency  $\eta$  a continuous efficiency curve of the format as in [Equation 1] below shall be obtained by statistical curve fitting of the test point results, using the least square method.

$$\eta = \eta_0 - a_1 \times T_m^* - a_2 \times G (T_m^*)^2 \quad [\text{Eq. 1}]$$

where

- $\eta_0$  is the zero-loss collector efficiency ( $\eta$  at  $T_m^*=0$ ), reference to  $T_m^*$  [-];
- $a_1$  is the heat loss coefficient at  $(T_m - T_a) = 0$  (first order coefficient), in  $\text{Wm}^{-2}\text{K}^{-1}$ ;
- $a_2$  is the temperature dependence of the heat loss coefficient (second order coefficient), in  $\text{Wm}^{-2}\text{K}^{-1}$ ;
- $T_m^*$  is the reduced temperature difference in  $\text{m}^2\text{KW}^{-1}$

with

$$T_m^* = (t_m - t_a) / G \quad [\text{Eq. 2}]$$

where

- $t_a$  is the ambient or surrounding air temperature
- $t_m$  is the mean temperature of the heat transfer fluid

with

$$t_m = t_{in} + 0,5 \times \Delta T \quad [\text{Eq. 3}]$$

where

<sup>7</sup> the instantaneous efficiency  $\eta$  in a test is measured from the product of *flowrate*, temperature increase over the collector and the specific heat of water divided by the solar irradiance input during the test.

<sup>8</sup> For instance, with water filled collectors and a test at  $T_a = 10^\circ C$  appropriate test values of  $T_m$  could be 10-35-60-85  $^\circ C$

- $t_{in}$  is the collector inlet temperature
- $\Delta T$  is temperature difference between fluid outlet and inlet ( $= t_e - t_{in}$ )<sup>9</sup>.

Unless specified differently, all tests shall be performed according to Best Testing Practice.

## INTEGRATED COLLECTOR STORAGE TESTS

In case of an Integrated Collector Storage ICS (e.g. ‘heat pipe’, vacuum-pipes directly coupled to tank, etc.) an alternative test is used, establishing the overall efficiency *etasol* of the collector+store combination during a 3 day test at maximum heat output, according to Best Testing Practice for this type of heat generator.

## AIR SOURCE HEAT PUMPS

Test points for air-source heat pumps are given in the table below.

**Table IV.2. Test points outdoor air-source HP**

Test	Results		Source temperature	low dT (minimum 1 K)			high dT (maximum 20 K)			Note
	power output	COP		T <sub>out</sub> dry bulb (wet bulb)	T <sub>return</sub>	T <sub>sys</sub>	T <sub>feed</sub>	T <sub>return</sub>	T <sub>sys</sub>	
	kW		°C	°C	°C	°C	°C	°C	°C	
<b>C</b>	<b>Php1</b>	<b>COP1</b>	<b>-7(-8)</b>	49	51	52	41	51	61	[3]
<b>A</b>	<b>Php2</b>	<b>COP2</b>	<b>2(1)</b>	40	41	42	33	41	49	
<b>B</b>	<b>Php3</b>	<b>COP3</b>	<b>7(6)</b>	34	35	36	30	35	40	
<b>D</b>	<b>Php4</b>	<b>COP4</b>	<b>12(11)</b>	27	28	29	26	28	30	
<b>E</b>	<b>Php5</b>	<b>COP5</b>	<b>-15(-17)</b>	57	59	61	49	59	69	[4]
<b>cyc</b>	<b>Phpcyc</b>	<b>COPcyc</b>	<b>12(11)</b>	As test point D, but cycling 6 minutes 'on', 24 minutes 'off'						[5]

[1]= Manufacturer to choose between low dT or high dT regime

[2]=For low dT regime the tolerance (permissible deviation of average value over testperiod) on T<sub>feed</sub> is 0,5K. For T<sub>sys</sub> and T<sub>return</sub> the tolerance is as indicated in table IV.1. For high dT regime the tolerance (permissible deviation of average value over testperiod) on T<sub>return</sub> is 0,5K. For T<sub>sys</sub> and T<sub>feed</sub> the tolerance is as indicated in table IV.1.

[3]=If binlimit>-7 then COP4=1 and Php4=1

[4]=Test point E only mandatory in case Colder climate is one of the designated climates

[5]=Test point 'cyc' and 'D' are used to determine the degradation factor.

<sup>9</sup>  $t_e$  is the collector outlet (exit) temperature. Note:  $t_{in}$  and  $t_e$  were previously known as  $T_{c,in}$  and  $T_{c,out}$  in the 2001 Edition of EN 12975-2

For HP compliance assessment the product shall at least meet the declared power output levels at the given source temperatures and the COP values shall be measured at the declared power output levels.

Testing is differentiated between fixed capacity, staged capacity and variable capacity as defined in document 3.

The following procedure applies for **fixed capacity units**:

1. Determine the (maximum) efficiency  $COP$  and the (maximum) output power  $Php$  at steady-state on-mode for each of the 4 or 5 test points. The COP and  $Php$  results are inputs in documents 4 and 6.
2. Perform one cyclic test at an outdoor dry bulb temperature of 12 °C. One cycle is 6 minutes in on-mode and 24 minutes in off mode, corresponding to approximately 20% part load conditions. Measure de  $COP$  value  $COP_{cyc}$  and the average heating power output over the test period  $Phpcyc$ .
3. Determine the efficiency degradation between cycling and steady state mode at outdoor temperature 12 °C<sup>10</sup>:  $dCOP = COP1 - COP_{cyc}$ .
4. Determine efficiency loss per kW of output heating power:  $Cd = dCOP / (Php1 - P_{cyc})$   
The  $Cd$ -value is to be reported in accordance with document 4 and will be used as an input in document 6.

The following procedure applies for **staged capacity units**:

1. Determine the heating power output  $Pc$  in kW and the electric power consumption  $Pe$  in kW at each of the two ‘stages’ of capacity control of the unit. The higher values are denominated  $Pc_1$  and  $Pe_1$ . The lower values are  $Pc_2$  and  $Pe_2$ . For a specific test point with heating power demand (‘load’)  $P_j$ , the fractions of  $Pc_1$  and  $Pc_2$  needed to reach  $P_j$  are  $t_1$  and  $t_2$  respectively, determined by the expressions

$$t_1 = (Pc_2 - P_j) / (Pc_2 - Pc_1) \text{ and}$$

$$t_2 = 1 - t_1$$

The aggregated COP value  $COP''_j$  for a test point in bin  $j$  is then  
 $COP''_j = (t_1 * Pc_1 + t_2 * Pc_2) / (t_1 * Pe_1 + t_2 * Pe_2)$

2. Subsequently a 2,5% correction is applied for the fact that it is staged and not a variable capacity unit (non-linearity), before the final value COP shall be used as an input in document 4 and document 6.

$$COP_j = 0,975 * COP''_j$$

3. If the smallest control step of the unit is higher than the required part load ratio (D and/or C and/or B), the  $COP$  at the required part load ratio is determined as for fixed capacity units. The  $Cd$ -value is to be reported in accordance with document 4 and will be used as an input in document 6.

<sup>10</sup> Can also be at 7 °C outdoor temperature, and using COP2 as a maximum load reference instead of COP1.

The following procedure applies for *variable capacity units*:

1. Perform the tests at the required part load ratios with the corresponding setting of the capacity control of the unit. The COP and  $P_{hp}$  results are inputs in documents 4 and 6.
2. If the electronic control of the unit does not allow obtaining the required part load ratio, the calculation procedure given for staged capacity units shall be applied.
3. If the smallest setting of the capacity control does not allow reaching one or several part load ratios, the COP at the required part load ratio(s) shall be calculated as for fixed capacity units. The  $C_d$ -value is to be reported in accordance with document 4 and will be used as an input in document 6.

## OTHER HEAT PUMPS

Other types of heat pumps shall be tested at the ambient heat conditions and test points as defined in document 3. The test points are directly used in the model. In addition the degradation factor  $C_d$  is determined through a cycling test as for air-source heat pumps.

## FOSSIL FUEL

The tables below give the *test points* for preferential (FOS) and non-preferential (FOSB) fossil fuel fired heat generators

**Table IV.3. Test points FOS**

Name	Results	Power input [1] kW	$T_{return}$ [2] oC	$T_{sys}$ [3] oC	$T_{feed}$ [3] oC	
I	$\eta_{1}$ [5]	$0,5t_d * P_{inmax}$	26	28	30	
II	$\eta_{2}$	$t_d * P_{inmax}$	30	35	40	
III	$\eta_{4}$	Pinmax	a)	60	70	80
			or b) [4]	45	55	65
IV	$\eta_{2hot}$	$t_d * P_{inmax}$	a)	60	70	80
			or b) [4]	45	55	65
V	$\eta_{1hot}$ [5]	$0,5t_d * P_{inmax}$	30	35	40	

[1]= If  $t_d$  of the product is larger than 30% then tests are to be performed at a default  $t_d$  value of 30%

[2]= Tolerance + 0,5 K

[3]= Tolerance as in Table IV.1

[4]= option b) is allowed only if the power output at Pinmax is lower than  $1,66P_{design}$ ; if option b) applies for point D then it shall also be used for point E

[5]= cycle time (50%'on'+ 50% 'off') is 10 minutes if  $t_d$  of the appliance is >60%, 20 minutes if  $t_d$  is >30% and 30 minutes if  $t_d$  <30%

**Table IV.4 . Test points FOSB\***

Name	Results	Power input	$T_{return}$	$T_{sys}^{**}$	$T_{feed}^{**}$
------	---------	-------------	--------------	----------------	-----------------

		kW	oC	oC	oC
<b>Ib</b>	<b>_etab1</b>	0,5td*Pinmaxb	<b>30</b>	<b>33-35</b>	<b>36-40</b>
<b>IIb</b>	<b>_etab2</b>	td*Pinmaxb	<b>45</b>	<b>55</b>	<b>65</b>
<b>IIIb</b>	<b>_etab4</b>	Pinmaxb	<b>60</b>	<b>70</b>	<b>80</b>

\*=mandatory for all load profiles

The table IV.5 below gives the *input points* to be reported for the designated load profiles in accordance with document 4 and with the inputs to be used in document 6.

**Table IV.5. Input points FOS an FOSB**

Input	Tsys FOS [1]	Tsys FOSB [2]	dT (fixed) [3]	dT (var.) [4]	Heating power output in kW							
					XS	S	M	L	XL	XXL	3XL	4XL
<b>eta(b)4</b>	70	70	20	20	5,8	8,8	13,3	20	30	45	66	101
<b>eta(b)3</b>	54	54	12	20 [5]	3,5	5,3	8,0	12	18	27	40	61
<b>eta(b)2</b>	33	45	4	10	1,1	1,6	2,4	3,6	5,4	8	12	18
<b>eta(b)1</b>	28	33	2	4	0,5	0,8	1,2	1,8	2,7	4	6	9

[1]= Applies to preferential fossil-fuel fired heat generator

[2]= Applies to non-preferential fossil-fuel fired heat generator

[3]= Temperature difference in K between Tfeed and Treturn with Tsys as middle value, in case of a fixed speed circulator (PMP=3,4)

[4]= Temperature difference in K between Tfeed and Treturn with Tsys as middle value, in case of a fixed speed circulator (PMP=1,2,5)

[5]= If manufacturer gives a warranty on the heat exchanger of at least 10 years, this value may be higher, i.e. up to 40 K

In case of a staged capacity unit the efficiency values shall be diminished by 0,025.

The inputs at the input points in Table IV.5 shall be determined through inter-/extrapolation of the test results from the conditions in Tables IV.3 and IV.4 for the designated load profiles. The manufacturer can declare up to 3 designated load profiles in total with those test results.

## COGENERATION

In case of CHP being part of the product configuration it shall be tested as a preferential fossil fuel fired heat generator FOS, with the heating efficiency values as mentioned in table IV.3 and inter/extrapolated to arrive at the input values as specified in table IV.5. Furthermore, during the test the electric power output is measured and reported as the ratio of electric power output to ‘heat’ (fossil fuel GCV) input. These test results are then used –through inter-/extrapolation—to arrive at the values of \_chp4, \_chp3, \_chp2 and \_chp1 at the input points specified in table IV.5.

## COMBI-BOILER

Testing and calculation method for the assessment of *combitrans*, to be used as an input for combi-boiler water heating efficiency etawh defined in document 3:

1. Determine heat capacity in kWh/K of device  $c_{dev}$  and hot water content  $c_{water}$  (through calculation)
2. Make sure boiler and device are at ambient temperature  $T_a$ .
3. Fill device with cold water  $T_{cold}$  of 10 °C, immediately run boiler in space heating mode at part load (can be combined with efficiency test in space heating) for 20 minutes (load weighted average time between draw-offs for most tapping patterns M and higher),
4. Stop the boiler for 20 minutes (burner-off) to account for standing losses.
5. Draw-off water from the device until water temperature is again 10 °C. Measured result: Average water temperature of device  $T_{avg}$ , Energy content of drawn off water  $Q_{tapped}$  in kWh/draw-off
6. If necessary correct result for heat content of the device at start:  $Q_{tappedcorr} = Q_{tapped} - (T_{ambient} - 10) * c_{dev}$ .  $T_{avg}$  is corrected accordingly.
7. Determine maximum annual capacity  $Q_{capdev}$  in kWh/a (25 draw-offs per day in heating season)  $Q_{capdev} = 25 * alldays * Q_{tappedcorr}$  in kWh/d. where  $alldays$  is the number of days in the heating season, i.e. 213, 183, 273 days for Average, Warmer and Colder climate respectively.
8. Calculate the 24h average heat store power capacity  $P_{store} = Q_{capdev} / allhrs$
9. From the reference net daily peak energy demand declared water heating load profile  $Q_{ref}$  in kWh/d (from document 4, table II.2) calculate the average power demand over the 15h tapping period with  $P_{tap} = 0,6 * Q_{ref} / 15$ .
10. From the annual flue gas losses in space heating mode  $Q_{flue}$  in kWh/a for the highest declared space heating load profile as determined in document 6, calculate the average loss over the heating season  $P_{flue} = Q_{flue} / allhrs$ .
11. The annual credit for the Passive Flue Heat Recovery Device  $combitrans$  in kWh/a is  $combitrans = allhrs * MIN(P_{store}; P_{tap}; P_{flue})$

## NO<sub>x</sub> EMISSIONS

NO<sub>x</sub> emissions are to be tested in accordance with best testing practice. Guidance documents are given in document 7.

## Document 6 Energy Efficiency Calculation Method

The mathematical model of the space heating boiler in this document (hereafter ‘the model’) calculates the specific energy efficiency *etas* from the input data given in document 4, Product Information requirements, Table II.4a in accordance with the definitions in document 3 and the testing methods and preliminary calculations in document 5.

The model is built top-down, with the most aggregated parameters first, followed by the parameters from which the aggregated parameters are built.

The model is divided in three parts:

- a **definition** section (eq. 1-14), giving the general definitions of efficiency, total energy consumption as well as the equations for informative issues as already defined in documents 3 and 4.
- a **heat balance** calculation (eq. 15-93), subdivided in
  - a heat demand section (eq. 15-30), dealing with the net space heating demand  $L_h$  (Eq. 15) that follows from the choice of the load profile and the so-called system losses  $L_{sys}$  (Eq. 16-30) that in part depend on the characteristics of the boiler and in part on other installation characteristics that are treated as constants. The system losses are fluctuation losses (Eq. 17-19), stratification losses (Eq. 20-21), distribution losses (Eq. 22-23), losses of buffers (Eq. 24-25), the losses from not optimally utilizing the night-setback potential  $Q_{tim}$  (Eq. 25-28) and finally losses or gains related to controls (Eq. 29-30).
  - a heat supply section (Eq. 30-93), calculating the contribution of each of the possible heat generator types SOL (eq. 32-57), HP (eq. 58-86), ELBU (eq. 87), FOS (eq. 88-90) and FOSB (eq. 91-93) in terms of their annual heating energy output ‘L’ in kWh/a. For FOS and FOSB this entails a simple capacity calculation, but SOL-output depends on the solar irradiance during the heating season – calculated with monthly inputs—and air-source HP outputs depends on the outdoor air (source) temperature, calculated with the bin-method (see document 3).
- a **primary energy loss accounting** (eq. 94-183), subdivided in
  - heat generator losses (eq. 94- 164), usually –except for SOL and ELBU where a simple annual multiplier is sufficient—calculated per outdoor temperature bin, and using the data inputs from tests as defined in document 5;
  - auxiliary energy losses (eq. 164-175), calculated on an annual basis and possible CHP gain from electric power production during the heat generating processes (eq. 176-183).

For the most part the model is a simple case of energy accounting. The accounting is comprehensive, also featuring parameters that might be redundant but serve transparency and a future purpose in model maintenance, but uses mostly simple linear equations.

A special feature is the use of the bin-method -as described in document 3- and the fact that the equations for inter- (and extra)polation between data inputs from the tests are explicitly part of the model, e.g. in eq. 65-70 (HP), eq. 118-132 (FOS) and eq. 178-183 (CHP). This may seem unnecessarily complex, because a simple instruction to interpolate between test point values could fully define any intermediate points. But it allows for more robust

modelling -with also a check on the overall contribution of a testing point to the end-result- and it allows the relatively simple incorporation of the modelling of the system buffer BUF with FOS and CHP.

Another feature is the transition of the energy calculation from the monthly method for SOL to the bin-method for HP and any of the following heat generators in eq. 71-80. This conversion the calculated annual heat output from SOL ( $L_{sol}$ ) according to the monthly method is redistributed over the temperature bins, starting at the hour-bins with the highest temperature and ending when the accumulated value of  $L_{sol}$  is exhausted. The remaining heat demand profile is then 'offered' to HP and the following heat generators, in the order as described in document 3.

## NOMENCLATURE

Parameters are listed as they are used, i.e. in the heat balance (Table V.1) and in the primary energy loss accounting (Table V.2). Table V.3 gives the main test and data input names.

**Table V.1. Nomenclature: Heat Balance**

### HEAT (kWh/a)

	<b><u>demand total</u></b>	0
space heating demand	<b>L<sub>h</sub></b>	0
system losses	<b>L<sub>sys</sub></b>	0
	<i>of which</i>	
fluctuation losses	<b>Q<sub>fluct</sub></b>	0
stratification losses	<b>Q<sub>strat</sub></b>	0
distribution losses	<b>Q<sub>distr</sub></b>	0
buffer losses	<b>Q<sub>buf</sub></b>	0
timer losses	<b>Q<sub>tim</sub></b>	0
	<b><u>supply total</u></b>	0
generator useful heat	<b><u>L<sub>gen</sub></u></b>	0
	<i>of which</i>	
solar heat supply	<b>L<sub>sol</sub></b>	0
heat pump heat supply	<b>L<sub>hp</sub></b>	0
electric back-up heat supply	<b>L<sub>elbu</sub></b>	0
fossil fuel fired preferential generator heat supply	<b>L<sub>fos</sub></b>	0
non-preferential fossil fuel fired generator heat supply	<b>L<sub>fosb</sub></b>	0

**Balance:  $L_h + L_{sys} = L_{gen}$**



**Table V.2. Nomenclature Primary Energy Loss Accounting**

**PRIMARY ENERGY LOSSES (kWh/a)**

auxiliary primary energy consumption (from electricity) minus primary energy credit from electricity production	<b>Qel</b>	0
	<i>of which</i>	
auxiliary primary energy consumption (from electricity)	<b>Qaux</b>	0
	<i>of which in Wh/a electric</i>	
circulator pump electricity consumption	<b>Qpmp</b>	0
solar auxiliary electricity consumption for solar pump, controls, anti-frost device, partitioned to space heating	<b>Qsolaux</b>	0
heat pump electricity consumption for controls, anti-frost device and --if not included in COP-- source fan or source pump, partitioned to space heating	<b>Qhpaux</b>	0
preferential fossil fuel fired generator auxiliary electricity consumption for controls, combustion fan, etc.	<b>Qfosaux</b>	0
non-preferential fossil fuel fired generator auxiliary electricity consumption for controls, combustion fan, etc.	<b>Qfosbau</b>	0
electric energy production from heat-lid CHP device	<b>Qchp (negative)</b>	0
heat generator losses	<b>Qgen</b>	0
	<i>of which</i>	
solar gain (negative) losses	<b>Qsol</b>	0
heat pump gain (usually negative) losses	<b>Qhp</b>	0
electric resistance back-up heater losses from power generation	<b>Qelbu</b>	0
preferential fossil fuel fired generator heat losses	<b>Qfos</b>	0
	<i>of which</i>	
energy consumption pilot flame	<b>Qign</b>	0
envelope losses in off-mode	<b>Qenvoff</b>	0
fuel losses (purge losses, emission of non-combusted fuel)	<b>Qfuel</b>	0
envelope losses in on-mode	<b>Qenvon</b>	0
flue gas losses	<b>Qflue</b>	0
non- preferential fossil fuel fired generator heat losses (b)	<b>Qfosb</b>	0
	<i>of which</i>	
energy consumption pilot flame (b)	<b>Qignb</b>	0
envelope losses in off-mode (b)	<b>Qenvoffb</b>	0
fuel losses: purge heat losses, emission of non-combusted fuel) (b)	<b>Qfuelb</b>	0
envelope losses in on-mode (b)	<b>Qenvonb</b>	0
flue gas losses (b)	<b>Qflueb</b>	0

**TOTAL Qel + Qgen**

0

$$Efficiency\ etas = Lh / (Lh + Lsys + Qgen + Qel)$$

**Table V.3. Nomenclature energy, power, efficiency and time for heat and power generators**

<b>heat generator (Boolean)</b>	<b>SOL</b>	<b>HP</b>	<b>ELBU</b>	<b>FOS</b>	<b>FOSB</b>	<b>CHP</b>
<b><u>Energy in kWh/a</u></b>						
instantaneous heat input (GCV of fuel)				Q <sub>in</sub>	Q <sub>inb</sub>	
primary energy loss total or per period/bin	Q <sub>sol</sub>	Q <sub>hp</sub>	Q <sub>elbu</sub>	Q <sub>fos</sub>	Q <sub>fosb</sub>	
useful output	L <sub>sol</sub>	L <sub>hp</sub>	L <sub>elbu</sub>	L <sub>fos</sub>	L <sub>fosb</sub>	
<b><u>Power in kW</u></b>						
maximum heat input in kWh/h upper heating value of fuel (GCV)				Pinmax	Pinmaxb	
heat demand remaining after SOL, HP, FOS	Prs	Prh		Prf		
<b><u>Efficiency (output/input) test points</u></b>						
cold climate only: -15 °C test point		COP5				
efficiency at maximum heat demand (load)	eta_0, a_1, a_2, IAM etasol	COP4	prim-energy	_eta4	_etab4	_chp4
efficiency at intermediate load		COP3				
efficiency at low load (or minimum steady state for FOS)		COP2		_eta2	_etab2	_chp2
efficiency at very low load (or 50% minimum steady state for FOS)		COP1		_eta1	_etab1	_chp1
extra test point cycling		COPcyc				
extra test point multiple load profiles 1				_eta2hot		_chp2hot
extra test point multiple load profiles 2				_eta1hot		_chp1hot
<b><u>Efficiency (output/input) input points</u></b>						
arrays of powers ( input points from tests)		Php		Pfos	Pfosb	chp
cold climate only: -15 °C		COP5 (Php5)				
efficiency (power) at maximum heat input		COP4 (Php4)		eta4 (Pfos4)	etab4 (Pfosb4)	chp4
efficiency (power) at design conditions		COP3 (Php3)		eta3 (Pfos3)	etab3 (Pfosb3)	chp3
efficiency (power) at minimum heat input (steady state)		COP2 (Php2)		eta2 (Pfos2)	etab2 (Pfosb2)	chp2
efficiency at very low load (or 50% minimum steady state for FOS)		COP1 (Php1)		eta1 (Pfos1)	etab1 (Pfosb1)	chp1
zero load 'efficiency'		COP0 (Php0)		eta4 (Pfos4)	etab4 (Pfosb4)	chp0
<b><u>Other</u></b>						
multipliers interpolation		w		b	bb	b
<b>hours in on mode</b>	solhrs	hphrs		foshrs	fosbhrs	foshrs
<b>hours in heating season</b>	allhrs					

## MODEL: Energy efficiency calculation

### DEFINITION SPECIFIC EFFICIENCY

#### **Select Load Profile**

Pdesign=[3,5; 5,3; 8; 12; 18; 27; 40; 60]

=[XS; S; M; L; XL; XXL; 3XL; 4XL]

*derived parameters:*

Pradnom=1,66Pdesign

nomflow=86,2Pradnom=143,1Pdesign

Fexist=10,87Pdesign

Fnew=28,57Pdesign

1
---

2
---

3
---

4
---

5
---

**Select climate** (only if SOL=1 and/or HP=1 & air-source; otherwise climate=1 only)

climate= [1;2;3]= [Average; Warmer; Colder]

6
---

*Load Profile Permitted (condition at climate=1 only)*

IF(OR(ELBU;Pmaxdesign>Pdesign); "permitted"; "not permitted")

Pmaxdesign=FOS\*\_eta4\*Pinmax+FOSB\*\_etab4\*Pinmaxb+HP\*Php4\*IF(binlimit<=-7;1;0)

7
---

8
---

#### **Specific seasonal efficiency**

**etas=Lh/(Lh+Lsys+Qgen+Qel)**

*for SOL=1 and/or HP=1 & air-source only, calculate*

etasA=Lh/QtotA

etasW=Lh/QtotW

etasC=Lh/QtotC

QtotA=Lh+LsysA+QgenA+Qel

QtotW=Lh+LsysW+QgenW+QelW

QtotC=Lh+LsysC+QgenC+QelC

9
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10
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11
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12
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13
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14
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### HEAT BALANCE

#### Heat Demand

**Lh=1000Pdesign**

**Lsys=Qfluct+Qstrat+Qdistr+Qbuf+Qtim+Qctrl**

*(climate specific)*

**Qfluct= Lh\*(Cfluct+ cband\*4%)**

Cfluct=2%

cband=BUF\*0,1+ELBU\*(1-HP)\*(1-FOS)\*0,1+(1-BUF)\*0,5\*(HP\*hptd\*Php3+(1-HP)\*td\*Pinmax\*\_eta4) / Pdesign

**Qstrat= Lh\*(Cstrat+cband\*2%)**

Cstrat=3%

**Qdistr= Lh\*(Cdistr+cband\*4%)**

Cdistr=5%

**Qbuf= 0,001\* allhrs\* {BUF\*(1-bufpos)\*Psbbuf\*(60 - (6+(bufpos/0,55)\*14) + SOL\*usesol\*(1-solpos)\*Psbsol\*(60 - (6+(bufpos/0,55)\*14) }**

*(climate specific)*

*allhrs=CHOOSE (climate; 4392;5124;6552)*

15
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16
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17
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18
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19
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20
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21
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22
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23
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24
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25
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<b>Q<sub>tim</sub> = (1-TIM)*fractim*L<sub>h</sub>+TIM*fractim*L<sub>h</sub>*C<sub>tim</sub></b>	26																																																												
<i>(climate specific)</i>																																																													
fractim= CHOOSE (climate;0,136;0,163;0,121)	27																																																												
C <sub>tim</sub> =TAN((1-reheat)*PI()/2)/TAN(0,77*PI()/2)	28																																																												
reheat is declared input defined as reheat= Preheat/Pradnom with boundaries																																																													
Preheat maximum is MIN(Pradnom; Pmaxdesign)) and reheat minimum 0,23																																																													
<b>Q<sub>ctrl</sub> = L<sub>h</sub>*c<sub>ctrl</sub></b>	29																																																												
c <sub>ctrl</sub> = CHOOSE(CTRL;0,03;0,01;0;-0,03;-0,05)	30																																																												
<b>Heat Supply</b>																																																													
<b>L<sub>gen</sub> = L<sub>sol</sub>+L<sub>hp</sub>+L<sub>elbu</sub>+L<sub>fos</sub>+L<sub>fosb</sub></b>	31																																																												
<i>(climate specific)</i>																																																													
<b>L<sub>sol</sub> = SOL*usesol*CHOOSE(ICS;SUM(L<sub>sol_tm</sub>);SUM(L<sub>solics_tm</sub>))</b>	32																																																												
usesol= 1-SOLCOMBI*((1-HPCOMBI)+0,7*HPCOMBI)*L <sub>w</sub> / (L <sub>h</sub> +L <sub>sys</sub> +L <sub>w</sub> )	33																																																												
L <sub>w</sub> = 213*50%*	34																																																												
*CHOOSE [waterload; 2,1; 2,1; 2,1; 5,85; 11,66; 19,07; 24,53; 46,76; 93,52]																																																													
ICS=[0;1]=[no;yes] integrated collector storage	35																																																												
L <sub>sol_tm</sub> =MAX(0; L <sub>tm</sub> *(L <sub>h</sub> +L <sub>sys</sub> )) *	36																																																												
* (1,029*Y <sub>tm</sub> - 0,065*X <sub>tm</sub> - 0,245*Y <sub>tm</sub> <sup>2</sup> + 0,0018 * X <sub>tm</sub> <sup>2</sup> + 0,0215*Y <sub>tm</sub> <sup>3</sup> )																																																													
L <sub>tm</sub> = CHOOSE(climate; LA <sub>tm</sub> ; LW <sub>tm</sub> ; LC <sub>tm</sub> )	37																																																												
LA <sub>tm</sub> = (L <sub>h</sub> +L <sub>sys</sub> )*	38																																																												
LW <sub>tm</sub> = (L <sub>h</sub> +L <sub>sys</sub> )*	39																																																												
LC <sub>tm</sub> = (L <sub>h</sub> +L <sub>sys</sub> )*	40																																																												
	<table border="1"> <tr> <td>0,20</td><td>0,20</td><td>0,13</td><td>0,06</td><td>0,06</td><td>0,16</td><td>0,19</td><td></td><td></td><td></td> </tr> <tr> <td>0,26</td><td>0,24</td><td>0,18</td><td>0,03</td><td>0,06</td><td>0,23</td><td></td><td></td><td></td><td></td> </tr> <tr> <td>0,17</td><td>0,17</td><td>0,14</td><td>0,09</td><td>0,04</td><td>0,03</td><td>0,08</td><td>0,12</td><td>0,16</td><td></td> </tr> </table>	0,20	0,20	0,13	0,06	0,06	0,16	0,19				0,26	0,24	0,18	0,03	0,06	0,23					0,17	0,17	0,14	0,09	0,04	0,03	0,08	0,12	0,16																															
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0,17	0,17	0,14	0,09	0,04	0,03	0,08	0,12	0,16																																																					
X <sub>tm</sub> = Asol*(a <sub>c</sub> + UL )*etaloop*(T <sub>refh</sub> - T <sub>out_tm</sub> ) * C <sub>cap</sub> * 0,732 / (L <sub>h</sub> +L <sub>sys</sub> )	41																																																												
Y <sub>tm</sub> = Asol*IAM*eta <sub>0</sub> *etaloop*qsolm <sub>tm</sub> *0,732 / (L <sub>h</sub> +L <sub>sys</sub> )	42																																																												
a <sub>c</sub> = a <sub>1</sub> +a <sub>2</sub> *40	43																																																												
UL = L <sub>pipesol</sub> *U <sub>pipesol</sub> /Asol	44																																																												
L <sub>pipesol</sub> =6	45																																																												
T <sub>refh</sub> =100	46																																																												
C <sub>cap</sub> = (75*Asol/Vsol) <sup>0,25</sup>	47																																																												
etaloop =1 - (eta <sub>0</sub> *Asol*a <sub>c</sub> )/U <sub>asol</sub>	48																																																												
T <sub>out_tm</sub> = CHOOSE(climate; T <sub>outA_tm</sub> ; T <sub>outW_tm</sub> ; T <sub>outC_tm</sub> )	49																																																												
T <sub>outA_tm</sub> =	50																																																												
T <sub>outW_tm</sub> =	51																																																												
T <sub>outC_tm</sub> =	52																																																												
qsolm <sub>tm</sub> = CHOOSE(climate; qsolmA <sub>tm</sub> ; qsolmW <sub>tm</sub> ; qsolmC <sub>tm</sub> )	53																																																												
qsolmA <sub>tm</sub> =	54																																																												
qsolmW <sub>tm</sub> =	55																																																												
qsolmC <sub>tm</sub> =	56																																																												
	<table border="1"> <tr> <td>2,8</td><td>2,6</td><td>7,4</td><td>12</td><td>12</td><td>5,6</td><td>3,2</td><td></td><td></td><td></td> </tr> <tr> <td>9,5</td><td>10</td><td>12</td><td>15</td><td>15</td><td>10</td><td></td><td></td><td></td><td></td> </tr> <tr> <td>-3,8</td><td>-4,1</td><td>-0,6</td><td>5,2</td><td>11</td><td>13</td><td>6,7</td><td>1,2</td><td>-3,5</td><td></td> </tr> <tr> <td>70</td><td>104</td><td>149</td><td>192</td><td>129</td><td>80</td><td>56</td><td></td><td></td><td></td> </tr> <tr> <td>129</td><td>138</td><td>182</td><td>227</td><td>126</td><td>110</td><td></td><td></td><td></td><td></td> </tr> <tr> <td>22</td><td>75</td><td>124</td><td>192</td><td>234</td><td>120</td><td>64</td><td>24</td><td>13</td><td></td> </tr> </table>	2,8	2,6	7,4	12	12	5,6	3,2				9,5	10	12	15	15	10					-3,8	-4,1	-0,6	5,2	11	13	6,7	1,2	-3,5		70	104	149	192	129	80	56				129	138	182	227	126	110					22	75	124	192	234	120	64	24	13	
2,8	2,6	7,4	12	12	5,6	3,2																																																							
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22	75	124	192	234	120	64	24	13																																																					

***In case of ICS/thermosiphon***

Lsolics\_tm= MIN(L\_tm\*(Lh+Lsys); 0,732\*Asol\*etasol\*qsolm\_tm) 57  
 etasol is ICS efficiency (solar input/ useful heat output) from best testing practice  
 qsolstest per m2 Asol is average global solar irradiation  
 during full test period (minimum 3 days)

**Lhp= HP\*usehp\*SUM(Lhp\_tp)** 58

usehp=1- HPCOMBI\*((1-SOLCOMBI)+0,3\*SOLCOMBI)\*Lw/ (Lh+Lsys+Lw) 59

Lhp\_tp= HP\*Pout\_tp\*hphrs\_tp 60

hphrs\_tp=HP\*IF(Pouthp\_tp>0;hr\_tp;0) 61

Pouthp\_tp=HP\*MIN(Poutmax\_tp; Prs\_tp) 62

Poutmaxhp\_tp= binlimit\_tp\*Pmaxhp 63

binlimit\_tp=IF(binlimit<=Tout\_tp;1;0) 64

Pmaxhp\_tp==Php1\*w1\_tp+Php2\*w2\_tp+Php3\*w3\_tp+Php4\*w4\_tp 65

Php1, Php2, Php3, Php4 are power outputs at test points tst  
 tst is array of Tout temperature of testbins. Tst=[tst1;tst2;tst3;tst;4]  
 with condition tst1>tst2>tst3>tst4 66

Pmaxhp\_tp is inter/extrapolation between these points, linear with Tout  
 using the following multipliers:

w1\_tp=IF(Tout\_tp>=tst1;1+(Tout\_tp-tst1)/(tst1-tst2); 67

IF(AND(Tout\_tp>tst2;Tout\_tp<tst1);1-(Tout\_tp-tst1)/(tst2-tst1);0))

w2\_tp=IF(AND(Tout\_tp<tst1;Tout\_tp>=tst2);(Tout\_tp-tst1)/(tst2-tst1); 68

IF(AND(Tout\_tp>tst3;Tout\_tp<tst2);1-(Tout\_tp-tst2)/(tst3-tst2);

IF(Tout\_tp>tst1;(Tout\_tp-tst1)/(tst2-tst1);0)))

w3\_tp=IF(AND(Tout\_tp<tst2;Tout\_tp>=tst3);(Tout\_tp-tst2)/(tst3-tst2); 69

IF(AND(Tout\_tp>tst4;Tout\_tp<tst3);1-(Tout\_tp-tst3)/(tst4-tst3);

IF(Tout\_tp<4;-(Tout\_tp-tst4)/(tst4-tst3);0)))

w4\_tp=IF(AND(Tout\_tp<tst3;Tout\_tp>=tst4);(Tout\_tp-tst3)/(tst4-tst3); 70

IF(AND(Tout\_tp<tst4);1+(Tout\_tp-tst4)/(tst4-tst3);0))

*in case of Cold climate eq. 69 and eq. 70 change; see endnote*

for all bins,except 'night'bin 71

Prs\_tp=IF(hr\_tp>0;(Lhsys\_tp-Lsol\_tp)/hr\_tp;0) 72

Lhsys\_tp= (Lh+Lsys)\*fracn\_tp 73

fracn\_tp=frac\_tp/SUM(frac\_tp) 74

frac\_tp=(1-TIM)\*fracs\_tp+TIM\*fracd\_tp 75

fracs\_tp=CHOOSE(climate; fracsA\_tp; fracsW\_tp; fracsC\_tp) 76

fracd\_tp=CHOOSE(climate; fracdA\_tp; fracdW\_tp; fracdC\_tp)

VALUES FROM TABLE I.1

Lsol\_tp=Lhsys\_tp\*IF(fracac\_tp<solfrac;1; 77

IF(fracac\_tp-frac\_tp<solfrac;(solfrac-fracac\_tp-frac\_tp)/frac\_tp;0)

solfrac=Lsol/(Lh+Lsys) 79

fracac=SUM(fracn\_0:fracn\_tp) 80

$hr\_tp=(1-TIM)*hrs\_tp+TIM*hrd\_tp$	81
$hrs\_tp=CHOOSE(climate; hrsA\_tp; hrsW\_tp; hrsC\_tp)$	82
$hrd\_tp=CHOOSE(climate; hrdA\_tp; hrdW\_tp; hrdC\_tp)$	83

VALUES FROM TABLE I.1

for 'night' bin: depends on TIM ; all expressions are to be multiplied with TIM  
following expressions are different from above

$Prs\_tp(night)=TIM*reheat*Pradnom$	84
$frac\_tp(night)=TIM*(0,01*fracd\_tp(night)+Ctim*0,136)$	85
substitute 0,136 with 0,161/0,121 in case of Warmer/Colder climate	86

$$hr\_tp(night)=IF(Prs\_tp>0;TIM*Lhsys\_tp/Prs\_tp;0)$$

Note that the 'night' outdoor temperatures are +1,+6, 0 °C for A, W, C climates

$Lelbu=ELBU*(Lh+Lsys-SOL*Lsol-HP*Lhp)$	87
--	----

$$Lfos=SUM(Lfos\_tp)$$

$Lfos\_tp=(1-ELBU)*FOS*IF(Prh\_tp>_eta4*Pinmax;_eta4*Pinmax*hr\_tp; Prh\_tp*hr\_tp)$	88
$Prh\_tp= Prs\_tp-Pouthp\_tp$	89
	90

$$Lfosb=(1-ELBU)*FOSB*(Lh+Lsys-SOL*Lsol-HP*Lhp-FOS*Lfos)$$

$Lfosb\_tp=Prf\_tp*hr\_tp$	91
$Prf\_tp=Prh\_tp -IF(hr\_tp>0;Lfos\_tp/hr\_tp;0)$	92
	93

### PRIMARY ENERGY LOSS ACCOUNTING

$Qgen=Qsol+Qhp+Qelbu+Qfos+Qfosb$	94
----------------------------------	----

$Qsol= SOL*- Lsol$	95
--------------------	----

$Qhp= HP*SUM(Qhp\_tp)-Lhp$	96
----------------------------	----

$Qhp\_tp=primenergyfac*Lhp\_tp/COP\_tp$	97
$COP\_tp=COP1*w1\_tp+COP2*w2\_tp+COP3*w3\_tp+COP4*w4\_tp$	98

$$- (Pouthp\_tp-Pmaxhp\_tp)*Cd\_tp$$

COP1, COP2, COP3, COP4 are steady state COP-values at test points;

COP<sub>tp</sub> is inter/extrapolation between these points, linear with Tout  
minus degradation factor Cd for cycling

Cd is measured at  $Php1=Pmax$  and  $COP1=COPmax$

$$Cd=(COPmax- COPcyc)/ (Pmax-Pcyc)$$

COP<sub>cyc</sub>, P<sub>cyc</sub> are measured at  $Php1/COP1$  conditions but with

6 minutes on/ 24 minutes off cycling

Cd is applied only if the part load is lower than the turndown ratio

$Cd\_tp=IF(AND(Pouthp\_tp>0; Pmaxhp\_tp>0);$ $IF(Pouthp\_tp/Pmaxhp\_tp<HPtd; Cd;0); 0)$	99
--	----

$primenergyfac=IF(HPELEC;2,5;1)$	100
----------------------------------	-----

HPELEC is declared input, with HPELEC=1=electric and  
HPELEC=0=fossil

Lhp\_tp is given from heat balance

$$Q_{elbu} = ELBU * 1,5 * L_{elbu} \quad 101$$

$$Q_{fos} = FOS * (Q_{ign} + Q_{envoff} + Q_{fuel} + Q_{envon} + Q_{flue}) \quad 102$$

$$Q_{ign} = (allhrs - foshrs) * P_{ign} \quad 103$$

$$Q_{envoff} = FOS * (allhrs - foshrs) * (1 - boilrecov) * P_{stby} * ((T_{sysoff} - 20) / 30)^{1,25} \quad 104$$

$$foshrs = \text{SUM}(foshrs\_tp) \quad 105$$

$$foshrs\_tp = Q_{out\_tp} / P_{out\_tp} \text{ (see table)} \quad 106$$

$$T_{sysoff} = 28 \quad 107$$

$$boilrecov = 0,55 \quad 108$$

$$P_{stby} = p\_stby * P_{inmax} \quad 109$$

$$Q_{fuel} = 0,001 * (Q_{in} - Q_{envon} - Q_{out}) \quad 110$$

$$Q_{envon} = foshrs * (1 - boilrecov) * P_{stby} * ((T_{syson} - 20) / 30)^{1,25} \quad 111$$

$$T_{syson} = 40 \quad 112$$

$$Q_{flue} = 0,999 * (Q_{in} - Q_{envon} - L_{fos}) \quad 113$$

$$Q_{in} = \text{SUM}(Q_{in\_tp}) \quad 114$$

void 115

$$Q_{in\_tp} = L_{fos\_tp} / \eta_{tp} \quad 116$$

$$L_{fos\_tp} = Prh\_tp * hrs\_tp \quad 117$$

Equation below shows how multipliers b0 to b4 are defined

the value of Prh\_tp is defined previously in equation 90.

$$Prh\_tp = b0\_tp * P_{fos0} + b1\_tp * P_{fos1} + b2\_tp * P_{fos2} + b3\_tp * P_{fos3} + b4\_tp * P_{fos4}$$

---


$$P_{fos0} = 0 \quad 118$$

$$P_{fos1} = \_eta1 * td * 0,5 * P_{inmax} \quad 119$$

$$P_{fos2} = \_eta2 * td * P_{inmax} \quad 120$$

$$P_{fos3} = \text{MIN}(\_eta4 * P_{inmax}; \_eta3 * P_{design}) \quad 121$$

$$P_{fos4} = \_eta4 * P_{inmax} \quad 122$$

$$b1\_tp = \text{IF}(\text{MATCH}(Prh\_tp; P_{fos}) = 2; Prh\_tp / (P_{fos2} - P_{fos1}); \quad 123$$

$$\text{IF}(\text{MATCH}(Prh\_tp; P_{fos}) = 1; 1 - b0\_tp; 0)$$

$$b2\_tp = \text{IF}(\text{MATCH}(Prh\_tp; P_{fos}) = 3; Prh\_tp / (P_{fos3} - P_{fos2}); \quad 124$$

$$\text{IF}(\text{MATCH}(Prh\_tp; P_{fos}) = 2; 1 - b1\_tp; 0)$$

$$b3\_tp = \text{IF}(\text{MATCH}(Prh\_tp; P_{fos}) = 4; Prh\_tp / (P_{fos4} - P_{fos3}); \quad 125$$

$$\text{IF}(\text{MATCH}(Prh\_tp; P_{fos}) = 3; 1 - b2\_tp; 0)$$

$$b4\_tp = \text{IF}(\text{MATCH}(Prh\_tp; P_{fos}) = 4; 1 - b3\_tp; 0) \quad 126$$

---


$$\eta_{tp} = \text{SUM}(P_{b\_tp} / \eta_{tp}) / \text{SUM}(P_{b\_tp}) \quad 127$$

$$\eta_{tp} = b0\_tp * \eta_{tp0} + b1\_tp * \eta_{tp1} + b2\_tp * \eta_{tp2} + b3\_tp * \eta_{tp3} + b4\_tp * \eta_{tp4} \quad 128$$

$$\eta_{tp0} = (1 - BUF) * (2 * \_eta1 - \_eta2) + \quad 129$$

$$+ BUF * \{ C_{buf} * \eta_{tp1} + (1 - C_{buf}) * (2 * \_eta1 - \_eta2) \}$$

$$\eta_{tp1} = (1 - BUF) * \_eta1 + BUF * \{ C_{buf} * \_eta2 + (1 - C_{buf}) * \_eta1 \} \quad 130$$

$$\eta_{tp2} = \_eta2 \quad 131$$

$$\eta_{tp3} = \_eta3 \quad 132$$

$$\eta_{tp4} = \text{IF}(pb(4) > pb(3); \_eta4; \_eta3) \quad 133$$

$C_{buf} = \text{MIN}(1; \text{MAX}(0; V_{buf} - 9P_{design}) / 41P_{design})$	134
<b><math>Q_{fosb} = \text{FOSB} * (Q_{ignb} + Q_{envoffb} + Q_{fuelb} + Q_{envonb} + Q_{flueb})</math></b>	135
$Q_{ignb} = \text{FOSB} * (\text{allhrs} - \text{onhrs}_b) * P_{ignb}$	136
$Q_{envoffb} = \text{FOSB} * (\text{allhrs} - \text{fosbhrs}) * (1 - \text{boilrecov}) * P_{stbyb} * ((T_{sysoffb} - 20) / 30)^{1,25}$	137
$\text{fosbhrs} = \text{SUM}(\text{fosbhrs}_{tp}) = Q_{outb\_tp} / P_{outb\_tp}$	138
$T_{sysoffb} = 28$	139
$Q_{fuelb} = \text{FOSB} * 0,001 * (Q_{inb} - Q_{envonb})$	140
$Q_{envonb} = \text{FOSB} * \text{fosbhrs} * (1 - \text{boilrecov}) * P_{stbyb} * ((T_{sysonb} - 20) / 30)^{1,25}$	141
$T_{sysonb} = 60$	142
$Q_{flueb} = 0,999 * (Q_{inb} - Q_{envonb} - L_{fosb})$	143
$Q_{inb} = \text{SUM}(Q_{inb\_tp})$	144
$Q_{inb\_tp} = L_{fosb\_tp} / \text{etab} / \text{tp}$	145
$L_{fosb\_tp} = P_{rf\_tp} * \text{hrs}_{tp}$	146
Equation below shows how multipliers bb0 to bb4 are defined the value of Prf_tp is defined previously in equation 93	
$P_{rf\_tp} = \text{bb0}_{tp} * P_{fosb0} + \text{bb1}_{tp} * P_{fosb1} + \text{bb2}_{tp} * P_{fosb2} + \text{bb3}_{tp} * P_{fosb3} + \text{bb4}_{tp} * P_{fosb4}$	
$P_{fosb0} = 0$	147
$P_{fosb1} = \_ \text{etab1} * \text{tdb} * 0,5 * P_{inmaxb}$	148
$P_{fosb2} = \_ \text{etab2} * \text{tdb} * P_{inmaxb}$	149
$P_{fosb3} = \text{MAX}(\_ \text{eta4} * P_{radnom}; P_{design})$	150
$P_{fosb4} = \_ \text{eta4b} * P_{inmaxb}$	151
$P_{fosb}$ is array [Pfosb0:Pfosb4]	152
$\text{bb0}_{tp} = \text{IF}(\text{MATCH}(P_{rf\_tp}; P_{fosb}) = 1; P_{rf\_tp} / (P_{fosb1} - P_{fosb0}); 0)$	153
$\text{bb1}_{tp} = \text{IF}(\text{MATCH}(P_{rf\_tp}; P_{fosb}) = 2; P_{rf\_tp} / (P_{fosb2} - P_{fosb1});$ $\text{IF}(\text{MATCH}(P_{rf\_tp}; P_{fosb}) = 1; 1 - \text{bb0}_{tp}; 0)$	154
$\text{bb2}_{tp} = \text{IF}(\text{MATCH}(P_{rf\_tp}; P_{fosb}) = 3; P_{rf\_tp} / (P_{fosb3} - P_{fosb2});$ $\text{IF}(\text{MATCH}(P_{rf\_tp}; P_{fosb}) = 2; 1 - \text{bb1}_{tp}; 0)$	155
$\text{bb3}_{tp} = \text{IF}(\text{MATCH}(P_{rf\_tp}; P_{fosb}) = 4; P_{rf\_tp} / (P_{fosb4} - P_{fosb3});$ $\text{IF}(\text{MATCH}(P_{rf\_tp}; P_{fosb}) = 3; 1 - \text{bb2}_{tp}; 0)$	156
$\text{bb4}_{tp} = \text{IF}(\text{MATCH}(P_{rf\_tp}; P_{fosb}) = 4; 1 - \text{bb3}_{tp}; 0)$	157
$\text{etab} = \text{SUM}(P_{bb\_tp} / \text{etab}_{tp}) / \text{SUM}(P_{bb\_tp})$	158
$\text{etab}_{tp} = \text{bb0} * \text{etab0} + \text{bb1} * \text{etab1} + \text{bb2} * \text{etab2} + \text{bb3} * \text{etab3} + \text{bb4} * \text{etab4}$	159
$\text{etab0} = 2 * \_ \text{etab1} - \_ \text{etab2}$	160
$\text{etab1} = \_ \text{etab1}$	161
$\text{etab2} = \_ \text{etab2}$	162
$\text{etab3} = \_ \text{etab3}$	163
$\text{etab4} = \text{IF}(P_{fosb4} > P_{fosb3}; \_ \text{etab4}; \_ \text{etab3})$	164
<b><math>Q_{el} = Q_{aux} - \text{CHP} * Q_{chp}</math></b>	165



$Q_{aux} = Q_{pmp} + (\text{primenergy} - \text{auxrecov}) * \{Q_{solaux} + Q_{hpaux} + Q_{fosaux} + Q_{fosbaux}\}$	166
$Q_{pmp} = \text{cpmp} * \text{tpump} * L_h$	167
$\text{tpump} = \text{CHOOSE}(\text{tpmp}; (\text{MAX}(\text{hponhrs}; \text{onhrs}) + 200) / \text{allhrs};$ $(\text{allhrs} - 0,33 * (\text{allhrs} - \text{MAX}(\text{hponhrs}; \text{onhrs}))) / \text{allhrs}; 1)$	168
$\text{cpmp} = \text{CHOOSE}(\text{PMP}; 0,02; 0,025; 0,04; 0,05; 0,06)$	169
$Q_{solaux} = \text{SOL} * 0,001 * \text{usesol} * (\text{solhrs} * \text{solaux} + (\text{allhrs} - \text{solhrs}) * \text{solsb})$	170
$\text{solhrs} = 0,163 * \text{allhrs}$	171
$Q_{hpaux} = \text{HP} * 0,001 * \text{usehp} * (\text{onhrshp} * \text{hpaux} + (\text{allhrs} - \text{onhrshp}) * \text{hpsb})$	172
$Q_{fosaux} = \text{FOS} * 0,001 * (\text{foshrs} * \text{fosaux} + (\text{allhrs} - \text{foshrs}) * \text{fossb})$	173
$\text{fosaux} = 0,5 * (\text{elmax} + \text{elmin})$	174
$Q_{fosbaux} = \text{fosbhrs} * \text{fosaux} + (\text{allhrs} - \text{fosbhrs}) * \text{fosbsb}$	175
$\text{fosbaux} = 0,5 * (\text{elmaxb} + \text{elminb})$	176
$Q_{chp} = \text{CHP} * \text{primenergy} * \text{SUM}(Q_{chp\_tp})$	177
$Q_{chp\_tp} = \text{foshrs\_tp} * P_{chp\_tp}$	178
$P_{chp\_tp} = b1\_tp * \text{chp1} + b2\_tp * \text{chp2} + b3\_tp * \text{chp3} + b4\_tp * \text{chp4}$	179
$\text{chp1} = (1 - \text{BUF}) * \_chp1 * 0,5 * \text{td} * \text{Pinmax} + \text{BUF} * (\text{CBuf} * \_chp2 * 0,5 * \text{td} * \text{Pinmax}$ $+ (1 - \text{Cbuf}) * \_chp1 * 0,5 * \text{td} * \text{Pinmax})$	180
$\text{chp2} = \_chp2 * \text{td} * \text{Pinmax}$	181
$\text{chp3} = \text{IF}(\_chp4 * \text{Pinmax} > P_{\text{design}}; \_chp3 * (P_{\text{design}} / \_eta3); \_chp4 * \text{Pinmax})$	182
$\text{chp4} = \_chp4 * \text{Pinmax}$	183

**Endnote:**

In case of a cold climate COP5 is added as a new test point and equations 69, 70 and 98 change as follows:

**Eq. 65**

$$P_{\text{maxhp\_tp}} = P_{\text{hp1}} * w1C\_tp + P_{\text{hp2}} * w2C\_tp + P_{\text{hp3}} * w3C\_tp + P_{\text{hp4}} * w4C\_tp + P_{\text{hp5}} * w5C\_tp$$

**Eq. 69**

$$w3C\_tp = \text{IF}(\text{AND}(\text{ToutC\_tp} < \text{tst2}; \text{ToutC\_tp} \geq \text{tst3}); (\text{ToutC\_tp} - \text{tst2}) / (\text{tst3} - \text{tst2});$$

$$\text{IF}(\text{AND}(\text{ToutC\_tp} > \text{tst4}; \text{ToutC\_tp} < \text{tst3}); 1 - (\text{ToutC\_tp} - \text{tst3}) / (\text{tst4} - \text{tst3});$$

$$\text{IF}(\text{ToutC\_tp} < 4; -(\text{ToutC\_tp} - \text{tst4}) / (\text{tst4} - \text{tst3}); 0))$$

**Eq. 70**

$$w4C\_tp = \text{IF}(\text{AND}(\text{ToutC\_tp} < \text{tst3}; \text{ToutC\_tp} \geq \text{tst4}); (\text{ToutC\_tp} - \text{tst3}) / (\text{tst4} - \text{tst3});$$

$$\text{IF}(\text{ToutC\_tp} < \text{tst4}; 1 - (\text{ToutC\_tp} - \text{tst4}) / (\text{tst5} - \text{tst4}); 0))$$

**add Eq. 70a**

$$w5C\_tp = \text{IF}(\text{AND}(\text{ToutC\_tp} < \text{tst4}; \text{ToutC\_tp} \geq \text{tst5}); (\text{ToutC\_tp} - \text{tst4}) / (\text{tst5} - \text{tst4});$$

$$\text{IF}(\text{ToutC\_tp} < \text{tst5}; 1 + (\text{ToutC\_tp} - \text{tst5}) / (\text{tst5} - \text{tst4}); 0))$$

**Eq. 98**

$$\text{COP\_tp} = (\text{COP1} * w1C\_tp + \text{COP2} * w2C\_tp + \text{COP3} * w3C\_tp + \text{COP4} * w4C\_tp + \text{COP5} * w5C\_tp) -$$

$$(\text{Pouthp\_tp} - P_{\text{maxhp\_tp}}) * C_d\_tp$$

**Document 7**  
**Verification procedure for market surveillance purposes**

Verification procedure tolerances for compliance assessment of the final outcome are for:

- declared efficiency *etas* values 5%.
- declared heating power output 5% and
- NOx emissions 10%

For the purposes of checking conformity with the requirements, the authorities of the Member States shall use the procedure set out in Annex II and reliable, accurate and reproducible measurement procedures, which take into account the generally recognised state of the art measurement methods, including methods set in documents the reference numbers of which have been published for that purpose in the Official Journal of the European Union.

Relevant documents:

**General and relating to heat demand (in numerical order)**

EN 442-2:1996; Radiators and convectors - Part 2: Test methods and rating

EN 12803:2006 Heating systems in buildings - Method for calculation of the design heat load

EN ISO 13790:2008. Thermal performance of buildings - Calculation of energy use for space heating and cooling. [replaces EN 832:1998]

EN 15232:2007; Energy performance of buildings - Impact of Building Automation, Controls and Building Management

EN 15316-2-1:2007, Heating systems in buildings - Method for calculation of system energy requirements and system efficiencies - Part 2 ( Space heating emission and distribution systems), 10.2005

EN 15316-2-3:2007, Heating systems in buildings - Method for calculation of system energy requirements and system efficiencies - Part 2-3: Space heating distribution systems, 10.2005

EN 15316-4:2007, Heating systems in buildings - Method for calculation of system energy requirements and system efficiencies - Part 4: Space heating generation systems; [parts 1 to 4 on combustion, heat pumps, solar, CHP respectively]

EN 15377:2008 Heating systems in buildings - Design of embedded water based surface heating and cooling systems – (Part 1: Determination of the design heating and cooling capacity; Part 2: Design, dimensioning and installation; Part 3: Optimizing for use of renewable energy sources)

**Relating to solar heat generators SOL (in numerical order)**

ISO 9459-2; 1995. Solar heating - Domestic water heating Systems - Part 2: Outdoor test methods for System Performance characterization and yearly Performance prediction of solar-only Systems

EN 15316-4-3; 2007. Heating systems in buildings - Method for calculation of system energy requirements and system efficiencies - Part 4-3: Space heating generation systems, thermal solar systems.

EN 12975-1:2006. THERMAL SOLAR SYSTEMS AND COMPONENTS. SOLAR COLLECTORS. PART 1: GENERAL REQUIREMENTS.

EN 12975-2; 2006. Thermal solar systems and components – Solar collectors - Part 2: Test methods

EN 12976-1:2000. Thermal solar systems and components - Factory made systems –. Part 1: General requirements.

EN 12976-2; 2006. Thermal solar systems and components - Factory made systems - Part 2: Test methods  
ISO 9459-5; 2007. Solar heating - Domestic water heating Systems - Part 5: System Performance Characterization by Means of Whole System Tests and Computer Simulation

ENV 12977-2; 2001. Thermal Solar Systems – Custom built systems—Part 2: Test Methods

EN 12977-3; 2008. Thermal Solar Systems – Custom built systems—Part 3: Performance test methods for solar water heater stores.

**Relating to heat pumps HP (in numerical order)**

EN 14511:2004, Air conditioners, liquid chilling packages and heat pumps with electrically driven compressors for space heating and cooling;

ISO 5151-2005, Non-ducted air conditioners and heat pumps – Testing and rating for performance;

EN 62301:2005. Household Electrical Appliances: Measurement of standby power.

EN 12102 :2008. Air conditioners, liquid chilling packages, heat pumps and dehumidifiers with electrically driven compressors for space heating and cooling - Measurement of airborne noise - Determination of the sound power.

**Relating to fossil-fuel fired heat generators FOS, FOSB (in numerical order)**

EN 267:1999. Forced draught oil burners - Definitions, requirements, testing, marking. [to be replaced by prEN 267:2005]

EN 297:1994. Gas-fired central heating boilers - Type B11 and B11BS boilers fitted with atmospheric burners of nominal heat input not exceeding 70 kW.

EN 303-1:1999. Heating boilers - Part 1: Heating boilers with forced draught burners - Terminology, general requirements, testing and marking.

EN 303-2:1998 en. Heating boilers - Part 2: Heating boilers with forced draught burners - Special requirements for boilers with atomizing oil burners.

EN 303-3:1998. Heating boilers - Part 3: Gas-fired central heating boilers - Assembly comprising a boiler body and a forced draught burner.

EN 303-4:1999. Heating boilers - Part 4: Heating boilers with forced draught burners - Special requirements for boilers with forced draught oil burners with outputs up to 70 kW and

a maximum operating pressure of 3 bar - Terminology, special requirements, testing and marking.

EN 303-6:2000 en. Heating boilers - Part 6: Heating boilers with forced draught burners - Specific requirements for the domestic hot water operation of combination boilers with atomizing oil burners of nominal heat input not exceeding 70 kW.

PrEN 303-7 dec. 2003. Heating boilers - Part 7: Gas-fired central heating boilers equipped with a forced draught burner of nominal heat output not exceeding 1000 kW.

EN 304:1993. Heating boilers - Test code for heating boilers for atomizing oil burners.

EN 483:1999 en. Gas-fired central heating boilers - Type C boilers of nominal heat input not exceeding 70 kW.

EN 625:1995. Gas-fired central heating boilers - Specific requirements for the domestic hot water operation of combination boilers of nominal heat input not exceeding 70 kW

EN 656:1999. Gas-fired central heating boilers - Type B boilers of nominal heat input exceeding 70 kW, but not exceeding 300 kW

EN 676:2003. Automatic forced draught burners for gaseous fuels

EN 677:1998 en. Gas-fired central heating boilers - Specific requirements for condensing boilers with a nominal heat input not exceeding 70 kW.

EN 13836:2006. Gas-fired central heating boilers - Type B boilers of nominal heat input exceeding 300 kW, but not exceeding 1000 kW .

EN 15034:2006. Heating boilers - Condensing heating boilers for fuel oil.

EN 15035:2006. Heating boilers - Room sealed operations for boilers for fuel oil.

EN 15456:2008 Heating boilers - Electrical power consumption for heat generators - System boundaries – Measurements

prEN 15502-1:2006 Gas-fired central heating boilers - Part 1: General requirements and tests;

#### **Relating to combi-boilers and water heating**

Commission Regulation XX/XX/EC on Dedicated Water Heaters

Building Research Establishment, Hayton.J., Assessment of passive flue heat recovery devices for recognition in SAP, 12 April 2007.

#### **Relating to Cylinders (in numerical order)**

EN 12897; 2006. Water Supply – Specification for indirectly heated unvented (closed) storage water heaters.

ENV 12977-3; 2001. Thermal solar systems and components – Custom built systems – Part 3: Performance characterisation of stores for solar heating systems

EN 15332: 2007. Heating boilers – Energetic assessment of hot water storage tanks (CEN/TC 57)

prEN 50440: 2005. Efficiency of domestic electrical storage water heaters

EN 60379: 2004. Methods for measuring the performance of electric storage water-heaters for household purposes

#### **Relating to NOx emissions of space heating boilers**

EN 483 ibid. (gas)

EN 656 ibid (gas)  
EN 267 ibid (oil)  
EN 303-2 ibid (oil)

**Document 8**  
**Indicative benchmarks for boilers**

The Benchmarks for the best environmental performance boilers are:

Energy efficiency –

- Non domestic heat-only Boilers 'specific efficiency' over 140 %
- CH heat only Boilers 'specific efficiency' over 122 %
- Cogeneration boilers 'specific efficiency' over 120 %

NOx Emissions –

- Heat production <35 mg/kWh GCV (gas) input (see document 4)
- Cogeneration <70mg/kWh GCV input

For other significant environmental parameters the lack of adequate test methods rules out the setting of benchmarks.

**Indicative benchmarks for boilers and space heating systems for other than reference systems (informative)**

Efficiency values in the underlying document are based on a single reference system for emitters and distribution systems, in order to create a level playing field and address the largest part of the current boiler market. The table gives estimated benchmarks in case of deviations from the reference.

<b><u>reference</u></b>	<b><u>Non-reference and effect on the energy efficiency performance (effect on efficiency*)</u></b>
Correct heat load calculation according to EN 12831:2003 or similar.	incorrect or no heat load calculation: up to - 10%. <sup>11</sup>
Design heating power ( $P_{design}$ ) in kW calculated with reheat correction 1,2 and temperature correction 1,15 (internal heat loss).	Other heating systems, e.g. not working with multi-zone setback strategy, may work with no or other corrections. This in itself does not lead to a lower annual heat demand, but a lower $P_{design}$ should be corrected by a higher full-load hour multiplier $hrs_{design}$ (now 1000).
Distribution losses for individual dwelling (multiple zones/rooms)	Local or single room/zone heating (+5%). Collective heating (-10%).
Heat transfer medium water (Low	steam (-10%),

<sup>11</sup> For oversizing fixed capacity units ca. 2,5% per space heating load class “off”. For variable capacity units with low turndown ratio less than 1% per space heating load class “off”. Example, a 21 kW ( $P_{inmax}$ ) fixed capacity combi-boiler in a small apartment is typically 4 classes “off” (XS instead of L), resulting in ca. 8-10% efficiency loss. The model gives an exact indication.

Temperature)	air-ducts (-10%), refrigerant (-5%).
LT radiators	floor/ wall heating (FOS, FOSB driven) +10% floor/ wall heating (HP driven) +20% HT radiators and/or convectors -10%
Multi-zone setback regime**	single-zone setback (-2%) no setback (-8 %, residential) no setback (-25%, commercial)
Room temperature control with modulating room-thermostat or weather controlled corrected by room-thermostat.	on-off thermostats or weather controlled without room temperature correction(-2%, equivalent of 'ext. T-control' option), only boiler thermostat (-20%)
Hydraulically balanced (manually) installation	unbalanced installations weather control without central room thermostat (-6%) unbalanced installations with central room thermostat (-4%). automatically balanced installation (+4%, equivalent of 'Multi TV' control option)

\*=note that values are indicative; the effects on the system efficiency depend very much on the local installation.

\*\*=in the model simplified to 'night-setback' but values derived from a regime with also day-setback periods for bathroom and bedrooms.